

Diffusion Stability of Mechanical Equilibrium in Compressible Isothermal Gases

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Abstract— This paper is presented stability condition of mechanical equilibrium for diffusion of compressible isothermal gases in a cylindrical domain. Two general cases of the divergent stable motions were considered when density depended on the conditions $div \vec{u} = 0$ and $div \vec{u} \neq 0$.

Stability criterion of mechanical equilibrium for the compressible gas mixture is proposed by defining continuous dependence of the velocity vector for the compressible flows in the Navier-Stokes problem from initial date. Using the parametrix method of theory nonlinear partial differential equations were obtained the velocity components for the transient compressible flows. Introduced stability condition for isothermal gases was predicted in the principal form by the energy conservation law and based on the transport equation for an appropriate convergent-divergent turbulent gas motion.

Index Terms—Navier-Stokes equations, compressible flow, parametrix method, stability condition, mechanical equilibrium, energy conservation law, diffusion in isothermal gases, external and internal forces, pressure distribution

I. INTRODUCTION

THIS paper is presented mathematical theory of diffusion stability for turbulent compressible flows given by the Navier-Stokes equations. The problem of stability condition of multi-component diffusion in gases has received widespread attention in mathematical and physical modeling of turbulent processes in isothermal gases. Mathematical theory of determining stability condition is fundamentally interesting and practical importance for engineering models of multi-component diffusion with the divergent-convergent turbulent effects. Experiences in studies of the isothermal diffusion for multi-component gas mixtures have shown that under certain conditions they can have a mechanical stability in which occurs equilibrium and is determined emergence of a subsequent gravitational regime [3]- [4]. Problems which relate to emergence of kinetic phase transitions, convection fluxes are traditionally studied in the framework of the hydrodynamic theory of heat and mass transfer [5]. Determination of regime change, description of the basic regularities of the development of convective perturbation can be implemented in the theory of stability [6]-[7]. Usually convection flows are studied in an environment

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when the compressibility of the medium is negligible and the perturbations of the phase state of the medium are small compared to their average values [6],[7]. This approach leads to simplification of the basic equations of hydrodynamics and has proved satisfactory for cases describing thermal convection of single-component and binary incompressible media [8]-[10]. In the papers [7]-[10] formal stability theory has been extended to diffusive mixing isothermal binary and ternary gas mixtures in channels of rectangular and cylindrical shapes. Comparison of experimental results of determining the mass transfer regime change is calculated within the experimental errors [10]. One of the main problems of sustainability issues in nonlinear approximation would be determining the conditions of mechanical equilibrium of the gas mixture, as its analysis offer up the characteristic values of the partial concentration gradients. In this paper it is assumed to obtain the stability condition of mechanical equilibrium for multi-component gas mixture in the presence of diffusion and cross effects of the divergent-convergent turbulence. The proposed model of stability condition of mechanical equilibrium is based on Lyapunov stability theory in terms uniform continuity for the Navier-Stokes problem where we have a perspective using some alternative approach which different from that is needed for studying stability condition in the general classical issues and deal with model problems for common phenomena of divergent-convergent turbulence. Here was defined the velocity vector and stability condition in terms Holder continuity which is indicated mechanics of the turbulent fluxes in isothermal gases.

II. GOVERNING EQUATION

To illustrate how works stability condition we note, that many problems formally exist for any Reynolds numbers and it can have an exact solution, but not all partial differential equation can describe real-nature phenomenon, therefore we will consider the basic model equations of hydrodynamics that correctly can be solved (existence, uniqueness and stability in terms of continuity). The requirement of stability is caused by the fact that physical evidence is usually determined from experiments and approximately, therefore we must be sure that the determined solution is the stability solution. This requirement of stability in terms of continuity seems to be important. Therefore first of all we must construct Lyapunov theory for the Navier-Stokes problem which will be a powerful determining method for defining the stability or instability domains for the turbulent motion.

Under stable flow we will understand continuous motion (Lyapunov stability). With respect to this requirement let us describe the used approach in the proof of existence and uniqueness of the Navier-Stokes problem under influence

divergence and rotation. The key idea of our research is to present existence, uniqueness and stability in terms of continuity. According to this idea we can get an integral representative for determining the velocity vector and the pressure distribution in case when stability criterion of mechanical equilibrium is determined by constructed weak solution in case continuous dependence initial data from defined solution of the Navier-Stokes problem. We involve this method to show that the velocity vector and an external force with respect to the pressure function exist and satisfy the energy conservation law. It has been found that a stability criterion is very useful in simplifying the processing and analysis of the experimental date. We use this method to show that the velocity vector and the external and internal forces with respect to the pressure function exist and satisfy the energy conservation law. Recalling from previous studies [11]-[12] idea of constructing stability condition was divided into two steps.

In the first step, the pressure function is excluded from the the Navier-Stokes equation by using rotor operator. According to this transformation we can get an integral representative for determining the velocity vector and the pressure distribution. We may assume that

$$\text{div } \vec{u} = 0$$

and

$$\text{rot } \vec{f} = 0, \text{rot } \vec{u}_0 = 0$$

Then we will get the following condition

$$\text{grad } \left(\frac{u^2}{2} + \frac{p}{\rho} - \Phi \right) = 0$$

where

$$\text{grad } \Phi(x, t) = -\vec{f}(x, t)$$

Due to this assertion we can find a weak solution and for the velocity vector influence of divergence from rotation in the Navier-Stokes problem. It is proved that under dependence of the energy conservation law from the external force there exists a unique velocity vector given by the integral representation. Due to appropriate a priory estimate here we get a stable solution for the Navier-Stokes problem which can be seen from “a priory” estimation of the Navier-Stokes problem.

In the second step we assume that $\text{div } \vec{u} \neq 0$. In this case under identical dependence of the energy conservation law from the external force we have got the integral representation. for the Navier-Stokes problem. Under above assumption $\text{div } \vec{u} \neq 0$ there exists a unique stable solution with the appropriate properties. This mathematical concept links with the identical energy conservation law and characterizes steady behavior of a converging-diverging turbulent gas motion.

The shape of turbulent region is determined by the properties which have shown stability of the velocity motion and the pressure distribution. Stabilizing mechanisms can be used to explain features observed in numerical simulations of turbulence. In the papers [11]-[12]

have been noted that instability behavior of the velocity vector and the pressure distribution depend on conditions of the initial data

$$\text{rot } \vec{f} = 0 \text{ or } \text{rot } \vec{u}_0 = 0.$$

We will exclude these cases of instability behavior and deal only with the stable turbulent motion.

III. MATHEMATICAL FORMULATION OF THE PROBLEM

Let us suppose that

$$\Omega = \{(r, \varphi, z) : 0 < r < \infty, 0 < \varphi < 2\pi, 0 < z < h\}, \Omega_T = \Omega \times (0 < t < \infty)$$

and consider the Navier -Stokes problem in the cylindrical coordinates (r, φ, z) (Fig. 1) in the following form

$$\frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \nabla) \vec{u} = -\frac{1}{\rho} \nabla p + \nu(x, t) \Delta \vec{u} + c(x, t) \nabla \text{div } \vec{u} + \vec{f}(x, t) \quad (1)$$

$$c(x, t) = \frac{4\nu(x, t)}{3} + \eta(x, t)$$

$$\vec{u}(r, \varphi, z, t) = \begin{cases} \vec{u}_v(r, \varphi, z, t) & \text{if } \text{div } \vec{u} = 0 \\ \vec{u}_\alpha(r, \varphi, z, t) & \text{if } \text{div } \vec{u} \neq 0 \end{cases}$$

in Ω_T with the initial conditions

$$\vec{u} \Big|_{t=0} = \vec{u}_0(r, \varphi, z) \text{ on } \Omega \quad (2)$$

and boundary conditions when the body does not react with the surrounding medium

$$\left[\frac{\partial \vec{u}}{\partial z} - h_1 \vec{u} \right]_{z=0} = 0 \quad (3)$$

$$\left[\frac{\partial \vec{u}}{\partial z} + h_2 \vec{u} \right]_{z=h} = 0 \quad (4)$$

$$\left[\frac{\partial \vec{u}}{\partial r} + h_3 \vec{u} \right]_{r=r_0} = 0 \quad (5)$$

We will look for the stable velocity vector

$$\vec{u}(r, \varphi, z, t) = u_r(r, \varphi, z, t) \vec{i} + u_\varphi(r, \varphi, z, t) \vec{j} + u_z(r, \varphi, z, t) \vec{k}$$

and the gas pressure field $p(r, \varphi, z, t)$ when

$$\vec{f}(r, \varphi, z, t) = f_r(r, \varphi, z, t) \vec{i} + f_\varphi(r, \varphi, z, t) \vec{j} + f_z(r, \varphi, z, t) \vec{k}$$

is the known vector function of the external and internal forces, ν is a kinematic viscosity, ρ is a gas density, η

is a dynamic viscosity which is related to the kinematic viscosity by $\eta = \rho\nu$, the symbol ∇ denotes the gradient with respect to the function, the symbol Δ denotes the three dimensional Laplace operator.

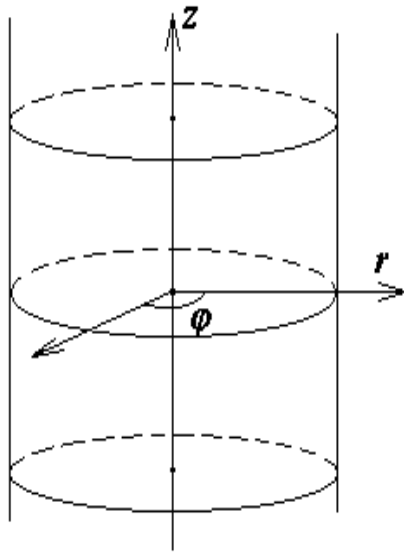


Fig. 1: Geometry of the problem

In the considered domain the initial boundary value problem (1)-(6) is concerned with the fundamental solutions for Poisson and heat conduction equations. Particular attention is paid to the integral representation of solutions with their initial values for the turbulent flux which is the basis of hydrodynamics.

IV. MAIN RESULTS AND DISCUSSION

A function $v(r, \varphi, z, t)$ defined on a bounded closed set S of R^3 is said to be Holder continuous of exponent α ($0 < \alpha < 1$) in S if there exists a const A such that

$$|v(x, t) - v(\xi, \tau)| \leq A(|x - \xi|^\alpha + |t - \tau|^{\alpha/2})$$

for all $(x, t) \in \Omega_T, (\xi, \tau) \in \Omega_T$ in S . Here $\nu(x, t)$ is a kinematic viscosity, $\rho(x, t)$ is a fluid density, the symbol ∇ denotes the gradient with respect to the function, the symbol Δ denotes the three dimensional Laplace operator, $\eta(x, t)$ is a dynamic viscosity which is related to the kinematic viscosity by the formula $\eta = \rho\nu$.

There we assume that

$$|\bar{u}| = \sqrt{u_1^2 + u_2^2 + u_3^2} \rightarrow 0 \text{ for } |x| = \sqrt{x_1^2 + x_2^2 + x_3^2} \rightarrow \infty$$

The initial value problem (1)-(5) is concerned with the fundamental solution for Poisson and heat conduction equations. Turbulent motion is supported by the subjected power from some external forces and initial velocity. The

shape of turbulent region is determined by the property which has shown stability or instability of the velocity motion and the pressure distribution. Stabilizing mechanisms have been advocated to explain features observed in numerical simulations of turbulence.

$$\frac{1}{2} \text{grad } \bar{u}^2 = [\bar{u} \times \text{rot} \bar{u}] + (\bar{u} \nabla) \bar{u} \quad (6)$$

we have got

$$\frac{\partial \bar{u}}{\partial t} + \text{grad} \left(\frac{P}{\rho} + \frac{1}{2} \bar{u}^2 \right) = [\bar{u} \times \text{rot} \bar{u}] + \nu(x, t) \Delta \bar{u} + \bar{f}(x, t) \quad (7)$$

Applying the expression

$$\text{grad} \left(\frac{u^2}{2} + \frac{P}{\rho} \right) + \bar{f} = 0$$

to the Navier-Stokes equations (3)-(5) we obtain the mathematical problem for heat equation

$$\frac{\partial \bar{u}}{\partial t} - \nu(x, t) \Delta \bar{u} = 2 \bar{f} \quad (8)$$

$$\text{div } \bar{u} = 0 \quad (9)$$

with the initial condition

$$\bar{u} |_{t=0} = \bar{u}_0(x) \quad (10)$$

Consider the heat equation (1) where the coefficient $\nu(x, t)$ is defined in a cylinder $\bar{D} \times [0, T] = \{(x, t); x \in \bar{D}, 0 \leq t \leq T\}$, \bar{D} is the closure of a bounded domain $D \in R^3$. Let for all $(x, t) \in \bar{D} \times [0, T], (\xi, \tau) \in \bar{D} \times [0, T]$ coefficient satisfies Holder conditions

$$|\nu(x, t) - \nu(\xi, \tau)| \leq |x - \xi|^\alpha + |t - \tau|^{\alpha/2}$$

Following the classical procedure [6] we can get solutions for the problem (8)-(10), (3)-(5) in the integral sum of the parabolic potentials

$$\begin{aligned} \bar{u}(r, z, t) = & \int_{\Omega} \bar{u}_0(r_1, z_1) G_\nu(r_1, z_1; r, z, t) d\Omega + \\ & + 2 \int_0^t d\tau \int_{\Omega} \bar{f}(r_1, z_1, \tau) G_\nu(r_1, z_1; r, z, t - \tau) d\Omega \end{aligned}$$

Fundamental solution $G(x - \xi, t)$ was obtained from integral equation

$$G(x - \xi, t) = g(x - \xi, t) + \int_{R^3} \int_0^T g(x - \eta, t - \sigma) \Phi_\nu(\eta, \xi, \sigma) d\eta d\sigma \quad (12)$$

where

$g(r, z; r_1, z_1, t)$ is the Green's function for the three dimensional finite domain $\Omega_T = \Omega \times (0 < t < \infty)$ where $\Omega = \{(r, \varphi, z) : 0 < r < \infty, 0 < \varphi < 2\pi, 0 < z < h\}$ which was defined in the following form

$$g_v(r, z, r_1, z_1, t) = \sum_{k,m=0}^{\infty} \frac{Z_{k,m}(z, z_1, t)}{2\beta t} e^{-\frac{(r^2+r_1^2)}{4\beta t}} I_0\left(\frac{rr_1}{2\beta t}\right) \quad (13)$$

$$\beta = \frac{\nu(\mu_k^2 + r_0^2 \lambda_m^2)}{r_0^2}$$

where

$$Z_{k,m}(z, z_1, t) = A_{k,m} e^{-\lambda_m \nu t} \sin(\lambda_m z_1 + z_m) \sin \lambda_m(z + z_m)$$

$$A_{k,m} = \frac{1}{r_0^2 J_0^2(\mu_k) \pi \left(h + \frac{(h_1 h_2 + \lambda_m^2)(h_1 + h_2)}{(h_1^2 + \lambda_m^2)(h_2^2 + \lambda_m^2)} \right) \left(1 + \frac{r_0^2 h_3^2 - h_3^2}{\mu_k^2} \right)}$$

$J_0(y)$ - Bessel function

μ_k is a positive solution of the transcendent equation

$$\mu_k J_0'(\mu_k) + r_0 h_3 J_0'(\mu_k) = 0$$

λ_m is a positive solution of the transcendent equation

$$cth \lambda_m h = \frac{\lambda_m^2 - h_1 h_2}{\lambda_m (h_1 + h_2)}$$

Parameter z_m is defined as

$$z_m = \text{artg} \frac{\lambda_m}{h_3}$$

Fundamental solution $G(r, z; r_1, z_1, t)$ has estimation in the following view

$$|G(r, z; r_1, z_1, t)| \leq \frac{e^{-\frac{r^2+r_1^2 r+(z-z_1)^2}{8\nu_0 t}}}{(\sqrt{\pi})^3 \nu_0^{3/2} t^{3/2}} I_0\left(\frac{rr_1}{4\nu_0 t}\right)$$

with its partial derivative in the following forms

$$\left| \frac{\partial}{\partial r} G_v \right| \leq \frac{e^{-\frac{r^2+r_1^2 r+(z-z_1)^2}{8\nu_0 t}}}{(\sqrt{\pi})^3 \nu_0^2 t^2} I_0\left(\frac{rr_1}{4\nu_0 t}\right)$$

$$\left| \frac{\partial}{\partial z} G_v \right| \leq \frac{e^{-\frac{r^2+r_1^2 r+(z-z_1)^2}{8\nu_0 t}}}{(\sqrt{\pi})^3 \nu_0^2 t^2} I_0\left(\frac{rr_1}{4\nu_0 t}\right)$$

$$(i = 1, 2, 3)$$

$I_0(y)$ is the modified zero order Bessel function of first kind.

Notice that stability in terms continuity and using the equation (8) was found unknown function $\Phi_v(x, t; \xi, \tau)$ as solution of the following Volterra-Fredholm integral equation

$$\Phi_v(x, t; \xi, \tau) = LZ_v(x, t; \xi, \tau) + \int_0^t \int_{R^3} LZ_v(x, t; \xi, \tau) \Phi_v(x, t; \xi, \tau) d\xi d\tau$$

$$LZ_v(x, t; \xi, \tau) = [v(x, t) - v(\xi, \tau)] \Delta_x Z_v(x, t; \xi, \tau)$$

by using successive approximation method

$$\Phi_v(x, t; \xi, \tau) = \sum_{n=1}^{\infty} (LZ_v)_n(x, t; \xi, \tau)$$

where

$$(LZ_v)_{n+1}(x, t; \xi, \tau) = \int_0^t \int_{R^3} (LZ_v)(x, t; \xi_1, \tau_1) (LZ_v)_n(\xi, \tau; \xi_1, \tau_1) d\xi_1 d\tau_1$$

For pressure function $p(x, t)$ we have got

$$\|p\|_{H_{\Omega_T}^{(1,0)}} \leq M_0 (\|\bar{u}_0\|_{H_{\Omega}^{(1)}} + \|\bar{f}\|_{L_2})$$

Consequently, we see that a stability of the turbulent flow depends on the condition (12).

Then there for the Navier-Stokes problem (1) - (5) exists a unique stable solutions in the form

$$\bar{u}(x, t) = \begin{cases} \bar{u}_v(x, t) = \bar{u}_0 * G_v + 2\bar{f} * G_v & \text{if } \text{div} \bar{u}(x, t) = 0 \\ \bar{u}_\alpha(x, t) = \text{grad} \{ \text{div} \bar{u}_0 * G_\alpha + 2\text{div} \bar{f} * G_\alpha \} & \text{if } \text{div} \bar{u}(x, t) \neq 0 \end{cases}$$

$$G_\alpha(r, z, r_1, z_1, t) = G_v(r, z, r_1, z_1, t) \Big|_{v=\alpha}$$

$$G_\alpha^*(r, z, t) = G_\alpha(r_1, z_1, t) * G_0(r - r_1, z - z_1)$$

and a unique scalar function of pressure $p(x, t)$ which satisfies energy conservation law

$$\frac{p}{\rho} + \frac{u^2}{2} - \text{div} \bar{f} * G_0(r - r_1, z - z_1) = 0 \quad (14)$$

where

$$u^2 = u_r^2 + u_\varphi^2 + u_z^2$$

$$G_0(r - r_1, z - z_1) = G_v(r, z, r_1, z_1, t) \Big|_{t=0}$$

Consequently, we see that a stability of the turbulent flow depends on the condition (14).

Moreover, there exists positive constant M_0 such that for all functions $\bar{u}(x,t) \in H^{2,1}(\Omega_T)$ and $p(x,t) \in H^{(1,0)}(\Omega_T)$ satisfy the following estimates for the velocity vector

$$\|\bar{u}\|_{H_{\Omega_T}^{(2,1)}} \leq \begin{cases} M_0(\|\bar{u}_0\|_{H_{\Omega}^{(1)}} + 2\|\vec{f}\|_{L_2}) & \text{if } \text{div}\bar{u}(x,t)=0 \\ M_0(\|\bar{u}_0\|_{H_{\Omega}^{(1)}} + 2\|\vec{f}\|_{H_{\Omega_T}^{(1,0)}}) & \text{if } \text{div}\bar{u}(x,t) \neq 0 \end{cases}$$

for the pressure function

$$\|p\|_{H_{\Omega_T}^{(1,0)}} \leq \begin{cases} M_0(\|\bar{u}_0\|_{H_{\Omega}^{(1)}} + 2\|\vec{f}\|_{L_2}) & \text{if } \text{div}\bar{u}(x,t)=0 \\ M_0(\|\bar{u}_0\|_{H_{\Omega}^{(1)}} + 2\|\vec{f}\|_{H_{\Omega_T}^{(1,0)}}) & \text{if } \text{div}\bar{u}(x,t) \neq 0 \end{cases}$$

V. RESULTS AND DISCUSSION

Let us gather and formulate main results about properties of the vector velocity and the scalar function of pressure.

Theorem1. Let $\bar{u}_0(x,t) \in H^{(1)}(\Omega)$ and $\vec{f}(x,t) \in L_2(\Omega_T)$ be periodic functions which satisfy conditions $\text{rot } \vec{f} = 0$, $\text{rot } \bar{u}_0 = 0$. Then there for the Navier-Stokes problem (1) - (5) exists a unique stable solutions in the form

$$\bar{u}(x,t) = \begin{cases} \bar{u}_v(x,t) = \bar{u}_0 * G_v + 2\vec{f} * G_v & \text{if } \text{div}\bar{u}(x,t)=0 \\ \bar{u}_\alpha(x,t) = \text{grad}\{\text{div}\bar{u}_0 * G_\alpha^* + 2\text{div}\vec{f} * G_\alpha^*\} & \text{if } \text{div}\bar{u}(x,t) \neq 0 \end{cases}$$

$$G_\alpha(r, z, r_1, z_1, t) = G_v(r, z, r_1, z_1, t) \Big|_{v=\alpha}$$

$$G_\alpha^*(r, z, t) = G_\alpha(r_1, z_1, t) * G_0(r - r_1, z - z_1)$$

and a unique scalar function of pressure $p(x,t)$ which satisfies energy conservation law

$$\frac{p}{\rho} + \frac{u^2}{2} - \text{div}\vec{f} * G_0(r - r_1, z - z_1) = 0$$

where

$$u^2 = u_r^2 + u_\phi^2 + u_z^2$$

$$G_0(r - r_1, z - z_1) = G_v(r, z, r_1, z_1, t) \Big|_{t=0}$$

Moreover, there exists positive constant M_0 such that for all functions $\bar{u}(x,t) \in H^{2,1}(\Omega_T)$ and $p(x,t) \in H^{(1,0)}(\Omega_T)$ satisfy the following estimates for the velocity vector

$$\|\bar{u}\|_{H_{\Omega_T}^{(2,1)}} \leq \begin{cases} M_0(\|\bar{u}_0\|_{H_{\Omega}^{(1)}} + 2\|\vec{f}\|_{L_2}) & \text{if } \text{div}\bar{u}(x,t)=0 \\ M_0(\|\bar{u}_0\|_{H_{\Omega}^{(1)}} + 2\|\vec{f}\|_{H_{\Omega_T}^{(1,0)}}) & \text{if } \text{div}\bar{u}(x,t) \neq 0 \end{cases}$$

for the pressure function

$$\|p\|_{H_{\Omega_T}^{(1,0)}} \leq \begin{cases} M_0(\|\bar{u}_0\|_{H_{\Omega}^{(1)}} + 2\|\vec{f}\|_{L_2}) & \text{if } \text{div}\bar{u}(x,t)=0 \\ M_0(\|\bar{u}_0\|_{H_{\Omega}^{(1)}} + 2\|\vec{f}\|_{H_{\Omega_T}^{(1,0)}}) & \text{if } \text{div}\bar{u}(x,t) \neq 0 \end{cases}$$

We can formulize this simple result that Bernoulli's equation is an consequence of the formula (19). Assume that $\text{rot } \vec{f} = 0$, $\text{rot } \bar{u}_0 = 0$ are satisfied. If $\vec{f} = C\bar{x} + \bar{d}$, where C can be chosen as matrix

$$C = \begin{pmatrix} \frac{c_1}{m} & 0 & 0 \\ 0 & \frac{c_2}{m} & 0 \\ 0 & 0 & -gh \end{pmatrix} \quad (15)$$

\bar{d} - a numerical vector, m - a body's mass, c_1, c_2 are independent constants which satisfy the condition $c_1 + c_2 \geq 0$, g is the acceleration of gravity, h is the height. Then fluid flow can be considered to be an incompressible flow which satisfies Bernoulli's equation

$$\frac{mp}{\rho} + \frac{mu^2}{2} + mgh = c \quad (16)$$

Here $c = c_1 + c_2$, $\frac{mp}{\rho}$ is a binding energy of the mass elements, $\frac{mu^2}{2}$ is a kinetic energy, mgh is a potential energy.

When initial density is a constant, divergence of the initial velocity is a constant and divergence of the external force depends on a given time t :

$$\rho_{0i} = \text{const}, \text{div}\bar{u}_{0i} = \text{const}, \text{div}\vec{f}_i = \text{div}\vec{f}_i(t)$$

Using properties of the fundamental solution

$$G_\alpha(r, z, r_1, z_1, t) = G_v(r, z, r_1, z_1, t) \Big|_{v=\alpha}$$

and species conservation law for n species we have got density for every species $i = 1, 2, \dots, n$ in the following form

$$\rho_i(t) = \rho_{0i} e^{-\left(\text{div}\bar{u}_{0i} + 2 \int_0^t \text{div}\vec{f}_i(\tau) d\tau\right)}$$

Similar comparative trend can be observed dependence on divergence from density. Total flux density can be found as sum

$$\rho(t) = \sum_{i=0}^n \rho_{0i} e^{-\left(\text{div} \vec{u}_{0i} + 2 \int_0^t \text{div} \vec{f}_i(\tau) d\tau\right)} \quad (17)$$

VI. CONCLUSION

Assume that a mathematical model of turbulent compressible flow was written as an initial value problem we have presented new analytic method which can be classified by stability balance condition. It is result when the velocity vector and the external and internal forces are expected to exist in finite domain. There are two unknown independent thermodynamic parameters (the velocity vector and the scalar function of pressure) which play a prominent role in the obtained integral representation of the velocity distribution for the description of the turbulent behavior of fluid motion. The Navier-Stokes equations have been the basis for description of turbulent phenomena where experimental selection of the regime turbulent fluctuation is costly and sometimes not always realizable process, therefore important argument for analytic research of the Navier-Stokes equation in the considered domain. There is presented mathematical approach which is based on the Green's function and required a good deal with the parabolic and elliptic potential theories. In processes dealing with governing equations the main point stressed that the velocity vector and the pressure function satisfy their balance criteria of stability motion which is the energy conservation law. In this research we use convenient procedure to investigate the Navier-Stokes equations which allows to use 'a priori' estimates for proof existence and uniqueness of weak solution. Weak formulation for the Navier-Stokes problem is based on the extension of idea to the case where the energy falls in the critical domain, due to the pressure transition. There we have essential feature of the Navier-Stokes equations. Moreover, basic concept our research is based on the weak formulation for the turbulent flows and introduced technique has been investigated in the Hilbert space. When we have stable solution then the weak formulation can be the classical formulation, so we can say under the stability condition we have the classical solution of the compressible Navier Stokes problem.

This research can be applied to engineering models for demonstrating technological applications of new analytic approach for modeling multicomponent compressible fluxes characterizing turbulent motion and playing a key role in the mass-heat transfer of the turbulent motion. Introduced approach leads to the conclusion that this submitted analytic solution would have been used for visualization the basic mechanism and the significant physical structure on the turbulence effects for turbulent influence of the pressure distribution from the external and internal forces in the considered cylindrical domain.

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