

# Analytical Analysis of a New Graphene-based Sensor for High-performance Biomolecule Sensing Applications

F. Djeflal, *Member, IAENG*, K. Tamersit, and M. Meguellati, *Member, IAENG*

**Abstract**—In this paper, an analytical investigation of a new graphene-based sensor called Dielectric Modulated Graphene Field Effect Transistor (DMG-FET), for high-performance biomolecule sensing applications, is developed and confirmed with numerical simulations. Transport drift-diffusion-based approach is used to develop the analytical models in order to study the DMG-FET behavior. The sensitivity of the proposed design is compared with that of conventional FET-based sensors. It has been shown that the proposed sensor has better electrical and scaling performance in comparison with the conventional design. This result makes the proposed design as a promising candidate to serve as a highly sensitive low-power and reliable graphene-based sensing applications. For that reason, the dielectric- modulated Graphene FET (DMGFET) provides a practical approach towards biomolecular detection that could be extended to other applications.

**Index Terms**— biomolecule sensing, dielectric, grapheme, sensitivity.

## I. INTRODUCTION

Recently, the Ion Sensitive FETs (ISFETs) sensors attract much attention in reliable and high performance applications for engineering and medical applications due to their reliability, low power consumption, non-destructive read-out of chemical and electrical information, high molecule detection range, and compatibility to standard CMOS technology [1-3]. However, with the progression of microelectronic industry and the increasing of the sensor performances, control of parasitic parameters and improvement of the sensor reliability against the biological and chemical variation of the neutral molecules are the biggest challenges in future embedded electronic systems for sensing and monitoring applications. Therefore, new design and materials should be developed in order to overcome these challenges. In this context, the use of Graphene-based material to design and fabricate these sensors may be considered as alternative for high performance and reliable monitoring applications. The importance of Graphene-based material is rising in microelectronic industry. This is mainly due to the low manufacturing costs of planar graphene and its excellent

electronic properties. Recently, several investigations have been proposed to analyze the Graphene-based devices and to make us better understanding of its physics behavior [4-6].

Dielectric modulated field effect transistors (DMFETs) are rising as a significant device for microelectronic applications due to its high saturation velocity, high carrier mobility and excellent charge transport [7-9]. Several works have investigated these devices [7-9]. However, these works have only been focused on studding the experimental aspects of these devices for silicon-based materials, where the analytical analysis, design methodologies and sensitivity behavior have not been taken into account, thus limiting the models and structures used by designers. Therefore, new analytical, materials and design approaches which capture and improve the sensitivity behavior, for high-performance biomolecule sensing applications, should be developed in order to build a complete graphene-based bimolecular sensor compact model and improved design for medical and engineering applications [11,12].

In this work, an analytical investigation of a new graphene-based sensor, for high-performance biomolecular sensing applications, is developed and confirmed by experimental validation. The sensitivity of the proposed design is compared with that of conventional Silicon (Si) FET-based sensors. It has been shown that the proposed sensor has better electrical and scaling performance in comparison with the conventional (Si) FET-based sensor.

## II. ANALYTICAL ANALYSIS

The present investigation suggests a new design called Dielectric Modulated Graphene Field Effect Transistor (DMG-FET) for high-performance biomolecule sensing applications, where the Dielectric region is introduced between the gate and the top-gate oxide. In Figure.1 (a and b), we show the cross sections of the proposed DMG-FET design. As it is shown in this figure, the detection is performed by the presence of air gap dielectric between the top gate and top-gate oxide.

Using an equivalent circuit analogy, a DMG-FET device can be represented by the Figure. 1c.

From the equivalent capacitive circuit,  $C_{T,EFF}$  and  $C_{Box}$  are the effective top gate capacitance ( $C_{Tox}$  in series with  $C_{gap}$ ) and the bottom oxide capacitance respectively.

where:

$$C_{T,EFF} = \varepsilon_{Top-ox} \varepsilon_{gap} / (\varepsilon_{gap} t_{Top-ox} + \varepsilon_{Top-ox} t_{gap})$$

$C_q$  represents the quantum capacitance of graphene.

$$C_q = k|V_C|$$

F. Djeflal is with the Laboratory of Advanced Electronic, Department of Electronics, LEPCM, University of Batna, 05000, Algeria (e-mail: faycaldzdz@hotmail.com, faycal.djeflal@univ-batna.dz).

K. Tamersit is with the Laboratory of Advanced Electronic, Department of Electronics, University of Batna, 05000, Algeria (e-mail: faycaldzdz@hotmail.com).

M. Meguellati is with the Laboratory of Advanced Electronic, Department of Electronics, University of Batna, 05000, Algeria (e-mail: m\_meguellati@yahoo.fr).

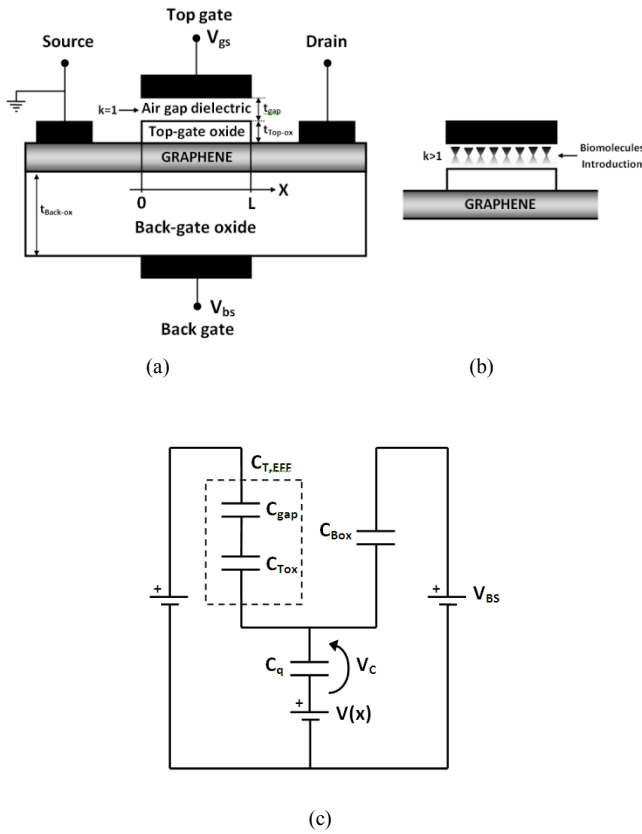


Figure 1. (a) cross section view of the double gate GFET transistor with air gap dielectric for the biodection before the biomolecule binding. (b) Cavity after biomolecules introduction. (c) Equivalent capacitive circuit of the graphene-based biotransistor.

where:  $k = (2q^2 / \pi)(q / (\hbar v_F))^2$  and  $v_F (= 10^6 \text{ m/s})$  is the Fermi velocity. The expression of  $C_q$  is convincing under the condition  $qV_C \gg k_B T$ .

The potential  $V(x)$  is the voltage drop in the graphene channel, which is equals to zero at the source end ( $x=0$ ) and equals to the drain–source voltage  $V_{ds}$  at the drain end ( $x=L$ ).

The overall net mobile sheet charge density in the graphene channel is defined [11] as

$$Q_c = q(p - n) = -(1/2)C_q V_C$$

where

$$V_C(x) = (V_{GS} - V(x)) \frac{C_{T,EFF}}{C_{T,EFF} + C_{Box} + \frac{1}{2}C_q} + (V_{BS} - V(x)) \frac{C_{Box}}{C_{T,EFF} + C_{Box} + \frac{1}{2}C_q}$$

with  $V_{GS} = V_{gs} - V_{gs0}$  and  $V_{BS} = V_{bs} - V_{bs0}$  are the top and back gate–source voltage overdrives, respectively. These quantities comprise work-function differences between the gates and the graphene channel, eventual charged interface states at the graphene/oxide interfaces, and intentional or unintentional doping of graphene.

To study the drain-current behavior in subthreshold regime a drift-diffusion carrier transport is assumed under the form  $I_{DS} = -qW\rho_c(x)v(x)$ , and  $\rho_c(x) = |Q_c|/q$  where  $W$  is the gate width,  $Q_c(x)$  is the free carrier sheet density in the channel at position  $x$ , which is mainly depends on the channel potential  $V(x)$ ; and  $v(x)$  represents the carrier drift

velocity in the channel. This latter can be expressed as,  $v = \mu E / (1 + \mu|E|/v_{sat})$  where  $v_{sat}$  is the saturation velocity,  $E$  and  $\mu$  represent the applied electric field and carrier mobility in the channel, respectively.

After some mathematical manipulations, the subthreshold current derived for our design can be expressed [13] as

$$I_{DS} = \frac{q\mu W \int_0^{V_{ds}} \rho_c dV}{L + \mu \left| \int_0^{V_{ds}} \frac{1}{v_{sat}} dV \right|}$$

where  $L$  represents the channel length. The subthreshold current derived for our design leads to:

$$I_{DS} = \frac{q\mu W \int_{V_{CS}}^{V_{CD}} \rho_c(V_C) \frac{dV}{dV_C} dV_C}{L + \mu \left| \int_{V_{CS}}^{V_{CD}} \frac{1}{v_{sat}(V_C)} \frac{dV}{dV_C} dV_C \right|}$$

where  $V_C$  is obtained from the expression of the channel potential,  $V_C(x)$ . This latter can be written as:

$$V_C = \frac{-(C_{T,EFF} + C_{Box}) + \sqrt{(C_{T,EFF} + C_{Box})^2 \pm 2k \left[ (V_{GS} - V + \frac{qN_f}{C_{T,EFF}}) C_{T,EFF} + (V_{BS} - V) C_{Box} \right]}}{\pm k}$$

where  $k$  is a constant, which takes a positive or negative sign,

$$\left( V_{GS} - V + \frac{qN_f}{C_{T,EFF}} \right) C_{T,EFF} + (V_{BS} - V) C_{Box} > 0 \quad (< 0),$$

respectively.

Also, both the channel potential at the source and drain sides  $V_{CS}$  and  $V_{CD}$  are determined by  $V_C(V=0)$  and  $V_C(V=V_{ds})$ , respectively. Moreover, the expression of  $V_C(x)$  leads to:

$$dV/dV_C = -(1 + kV_C \text{sgn}(V_C) / (C_{T,EFF} + C_{Box})), \quad \text{and}$$

$$\rho_c(V_C) = kV_C^2 / (2q) + \rho_0$$

From this latter, we can calculate the final subthreshold drain current model as,

$$I_{DS} = \mu \frac{W}{L_{eff}} \left[ q\rho_0 V_{ds} - \frac{k}{6} (V_{CD}^3 - V_{CS}^3) - \frac{k^2}{8(C_{T,EFF} + C_{Box})} (\text{sgn}(V_{CD}) V_{CD}^4 - \text{sgn}(V_{CS}) V_{CS}^4) \right]$$

with,

$$L_{eff} = L + \mu \frac{\sqrt{\pi}}{\Omega} \left[ -\frac{V_C}{2} \sqrt{\frac{kV_C^2}{2q} + \rho_0} - \frac{\rho_0 \log \left( 2 \left( \sqrt{\frac{k}{2q} \sqrt{\frac{kV_C^2}{2q} + \rho_0} + \frac{kV_C}{2q}} \right) \right)}{2 \sqrt{\frac{k}{2q}}} \right]_{V_{CS}}^{V_{CD}} - \text{sgn}(V_C) \frac{2q}{3(C_{T,EFF} + C_{Box})} \times \left( \left( \frac{kV_C^2}{2q} + \rho_0 \right)^{\frac{3}{2}} - \rho_0^{\frac{3}{2}} \right)$$

### III. RESULTS AND DISCUSSION

Figure 2 shows the variation of the obtained subthreshold current as function of applied gate-source voltage, where the dielectric material taken in this simulation is the silicon oxide. The simulated voltage range is extended beyond the experiment range to show the predictive behavior of the analytical model. The obtained results show good agreement in comparison with experimental measurements [15].

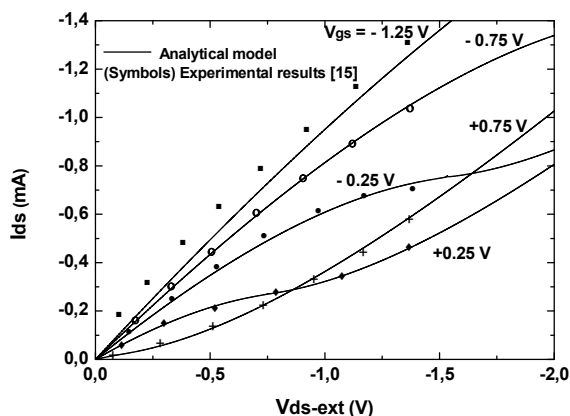
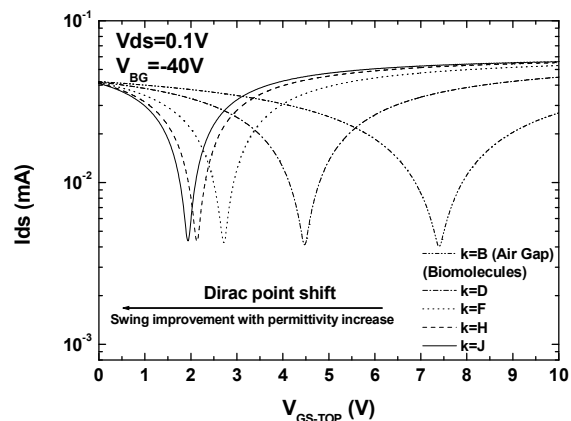
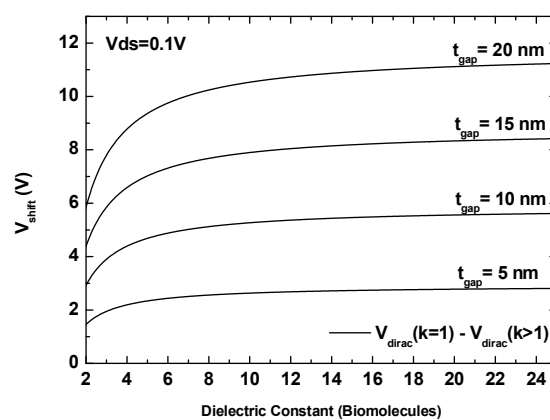


Figure 2. Output characteristics obtained from the analytical model compared with experimental results.

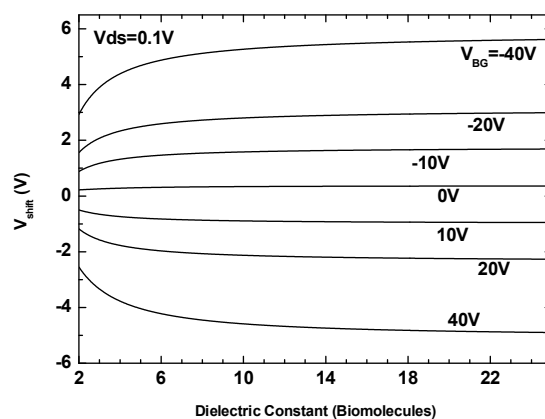
Figure.3 plots the proposed sensor behavior as function of different geometrical and electrical parameters. The impact of different parameters on the sensor sensitivity is also presented in this figure. Figure.3a shows the impact of the variation of the dielectric constant on the output I-V characteristics, where the shift of the Dirac-point in the negative direction is well observed. This shift is due to the increasing of the dielectric constant, which is mainly depends on the nature and the variation of biomolecular concentration. it is to note the that the main parameter which affects the shift in the Dirac-point is the top capacitance (CEFF). Figure.3b shows the variation of  $V_{shift}$  as function of dielectric constant for different nano-gap (cavity) values. It is shown that the increasing of the cavity width leads to an increasing in the sensitivity. Figure.3c plots the variation of  $V_{shift}$  as function of dielectric constant for different applied gate voltage values. It is clearly shown that  $V_{shift}$  is mainly depends on the applied gate voltage values, where its value increases when the applied voltage is increased. Therefore, high applied gate voltage is needed in order to obtain high sensor performances. Figure.3d shows the shift of the Dirac-point as function of negative biomolecule charges  $N_f$  located in the cavity region. For the proposed design, the output response of the sensor is linear with absorbed biomolecules concentration. It is clearly observed that DMG-FET has higher sensitivity. This means that DMG-FET has better electrical and scaling performances. From Figures 3a and 3b, we can observe that the sensor sensitivity cannot be affected by the channel length and the oxide thickness. It is to note that the same phenomenon can be observed for the impact of top-oxide dielectric constant.



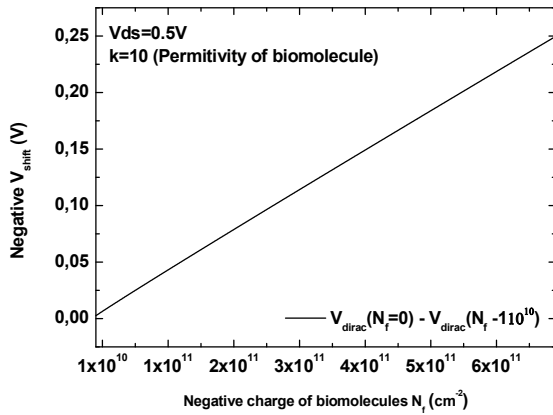
(a)



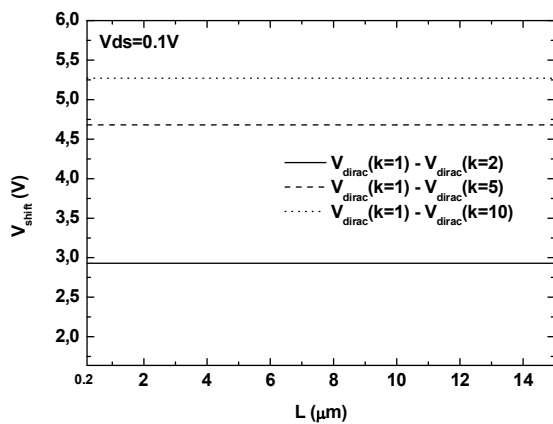
(b)



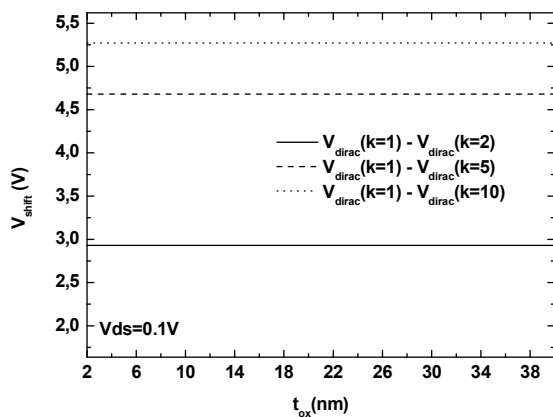
(c)



(d)



(e)



(f)

Figure 3. Output sensor parameters obtained from our analytical model (a) variation of Dirac point due to the dielectric constant variations (presence of biomolecular particles) (b)  $V_{shift}$  variation as function of dielectric constant for different nano-gap (cavity) values (c)  $V_{shift}$  variation as function of dielectric constant for different applied gate voltage values (d) shift of the Dirac point as function of biomolecular negative charge  $N_f$  located in the cavity region, (e) and (f) represent the variation of  $V_{shift}$  as function of channel length and the oxide thickness, respectively.

Due to the high performance provided by the proposed sensor (high sensitivity and voltage-shift linearity), the read

of the biomolecules concentration ( $N_f$ ) can be carried out by using a simple Read-out Circuit (RC), in which the threshold voltage is measured at a single point of the transfer characteristics, applying a specified current (in the order of ten  $\mu A$ ) to the sensor. Due to the simplicity of the Read-out Circuit, the RC configuration is suitable for practical low power applications

#### IV. CONCLUSION

In this paper, an analytical investigation of a new graphene-based sensor called Dielectric Modulated Graphene Field Effect Transistor (DMG-FET), for high-performance biomolecule sensing applications, is proposed. An analytical analysis comprising biomolecules concentration effect, drain current, threshold voltage shift and sensitivity behavior for DMG-FET has been developed. The sensitivity of the proposed has been investigated, and the impacts of variation in geometrical and electrical parameters have also studied. It is found that the sensitivity of the device can be increased by increasing the cavity thickness and the applied gate voltage. This result can be explained by the excellent sensitivity of the graphene against the variation of the top-electrostatic capacitance. The obtained results make DMG-FET a promising candidate for submicron, sensitive, low power, and reliable graphene-based biosensor.

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