

Transient Free TBSC Compensator for Dynamic Reactive Load with Closed Loop Control

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Abstract—Topology for reactive power compensation suitable for dynamic loads in closed loop is presented. The scheme consists of Thyristor Binary Switched Capacitor (TBSC) banks. TBSC is based on a chain of Thyristor Switched Capacitor (TSC) banks arranged in binary sequential manner. A transient free switching of TBSCs is carried out. Proposed topology allows stepless reactive power compensation for dynamic loads in very fast responding closed loop. Simulation results show that the proposed scheme can achieve reactive power compensation cycle to cycle basis and the harmonics contents of source are maintained at insignificant levels due to filtering action of TBSC.

Index Terms—Reactive power compensation, TBSC, transient free switching

I. INTRODUCTION

It is well documented in literature and through public discussions at various levels that a substantial power loss is taking place in our low voltage distribution systems on account of poor power factor, due to inadequate reactive power compensation facilities and their improper control. Switched LT capacitors can directly supply the reactive power of loads and improve the operating condition. Government of India has been insisting on shunt capacitor installations in massive way and encouraging the state electricity boards through Rural Electrification Corporation and various other financing bodies.

The expansion of rural power distribution systems with new connections and catering to agricultural sector in wide spread remote areas, giving rise to more inductive loads resulting in very low power factors. The voltages at the remote ends are low and the farmer's use high HP motors operating at low load levels with low efficiencies. This is giving rise to large losses in the distribution network. Thus there exists a great necessity to closely match reactive power with the load so as to improve power factor, boost the voltage and reduce the losses. The conventional methods of reactive power supply are through switched LT capacitors, mostly in equal steps in various automatic power factor controllers developed by number of companies.

In this paper, a more reliable, technically sound, fast acting and low cost scheme is presented by arranging the thyristor switched capacitor units in five binary sequential steps. This enables the reactive power variation with the least possible resolution.

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As there is reduction in loss with shunt compensation in the feeders, the efficiency increases and conservation of energy takes place. Besides the enhancement of transformer loading capability the shunt capacitor also improves the feeder performance, reduces voltage drop in the feeder and transformer, better voltage at load end, improves power factor and improves system security, increases over all efficiency, saves energy due to reduced system losses, avoids low power factor penalty, and reduces maximum demand charges.

II. DESIRABLE FEATURES

The desirable features of the proposed scheme are as follows:

- It maintains the power factor at the PCC to any specified value.
- It compensates for rapid variation in reactive power or voltages.
- Maximum compensation time is 20 msec.
- No transients or harmonics are allowed to be present due to fast selective instants of switching in well co-ordinated manner.
- It is adaptive in the sense that the amount of the compensation is determined and provided on a cycle by cycle basis.
- It can compensate each phase independently which makes ideal for unbalanced systems.
- Capacitors are sized in binary sequential ratio for minimum size of switching steps.
- The control strategy is error activated to match with the load reactive power for the chosen time interval.
- It eliminates possible over compensation and resulting leading power factor.
- It is flexible to choose required number of steps as per the resolution.
- Resolution can be made small with more number of steps.
- Simple in principle, elegant in usage and of low cost.
- Possible to incorporate the idea presented in the controllers for large size transformers at substations.

III. PROPOSED TOPOLOGY DESCRIPTION

This paper presents a simple topology, which is shown in Fig.1. The proposed scheme consists of Thyristor Switched Capacitor (TSC) banks in binary sequential steps known as Thyristor Binary Switched Capacitor (TBSC). This TBSC facilitates stepless control of reactive power closely matching with load requirements so as to maintain desired power factor. The proposed topology has following distinctive features:

- 1) TSC banks are arranged in Binary sequential steps to provide almost continuous reactive power compensation.
- 2) Transient free switching is obtained by pre-charging the capacitors to the negative/positive peak of supply voltage and firing the thyristors at the negative/positive peak of supply voltage.
- 3) It compensates for rapid variation in reactive power.

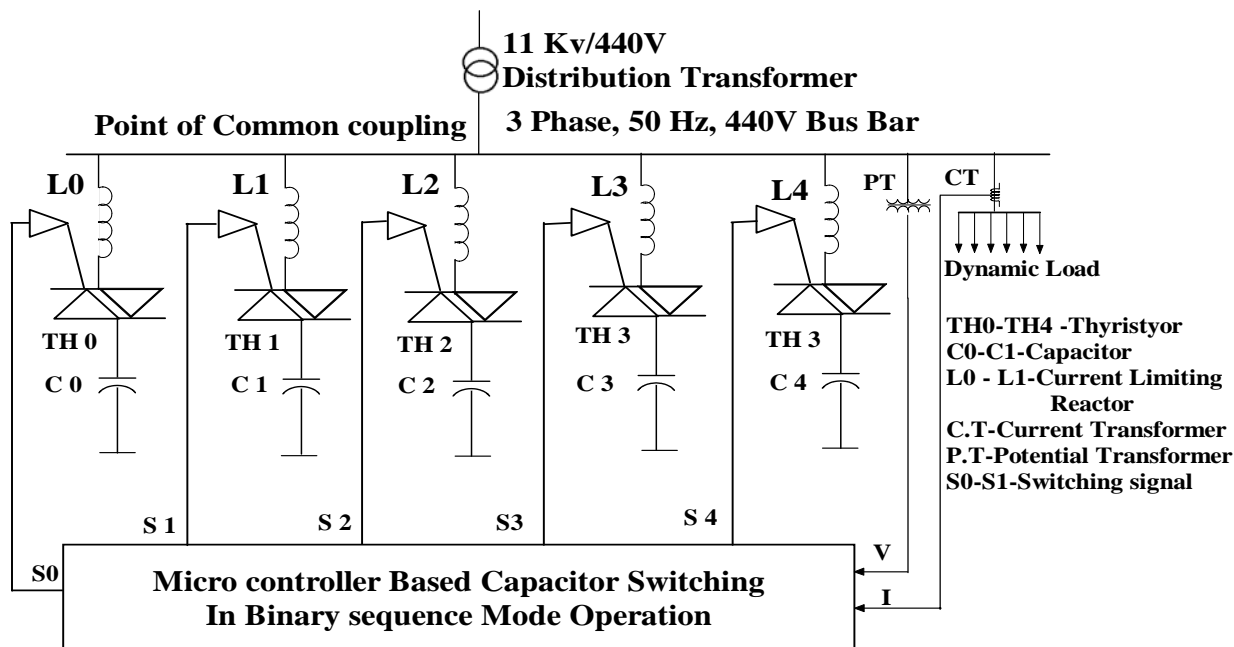


Fig.1 TBSC Compensator

4) Reactive power compensation is achieved in cycle by cycle basis

TBSC compensator connected at the point of common coupling (PCC) for reactive power compensation is shown in Fig.1. The operating principle of each equipment is analyzed in the following sections.

A. TBSC

TBSC consists of an anti-parallel connected thyristor and diode as a bidirectional switch in series with a capacitor and a current limiting small reactor. Transient free switching of capacitors is obtained by satisfying following two conditions.

- a. Firing the thyristors at the negative/positive peak of supply voltage.
- b. Precharging the Capacitors to the negative/positive peak of supply voltage

TSC current is sinusoidal and free from harmonics, thus eliminating the need for any filters. Small-series inductor is placed in series with capacitor. It serves following purposes

- a. It limits current transients during overvoltage conditions and when switching at incorrect instants or at the inappropriate voltage polarity.
- b. The chosen inductor magnitude gives a natural resonant frequency of many times the system nominal frequency. This ensures that the inductance neither creates a harmonic-resonant circuit with the network nor hampers the TSC control system.

In the proposed paper capacitor bank step values are chosen in binary sequence weights to make the resolution small. If such 'n' capacitor steps are used then 2^n different compensation levels can be provided [6]. In this paper five TBSC banks are arranged as 2.5: 5: 10: 20: 40 KVAR in star connected with neutral grounded configuration.

B. CONTROLLER

Controller is the heart of compensator. Voltage V and current I at PCC are sensed by Potential Transformer

(P.T.) & Current Transformer (C.T.) respectively and given to controller. Controller determines the value of reactive power required to achieve the desired power factor & then generates the control signals (gate signals) which are given to TBSC banks. By coordinating the control of TBSC, it is possible to obtain fully stepless control of reactive power in closed loop.

IV. CONTROLLER DESCRIPTION

A. TBSC Closed Loop Operation

A block diagram of reactive power compensator using TBSC banks is shown in Fig. 2. Reference reactive power, Q_{REF} is calculated from the desired power factor. Actual reactive power at PCC, Q_{ACTUAL} is calculated by sensing voltage and current at PCC by P.T. and C.T. respectively. Error between Q_{REF} and Q_{ACTUAL} is given to PI Controller. A Discrete PI Controller is used. Output of PI Controller is given to ADC and its output is given to TBSC banks in such a way that no transients occur. In this way closed loop operation of TBSC banks for reactive power compensation is achieved.

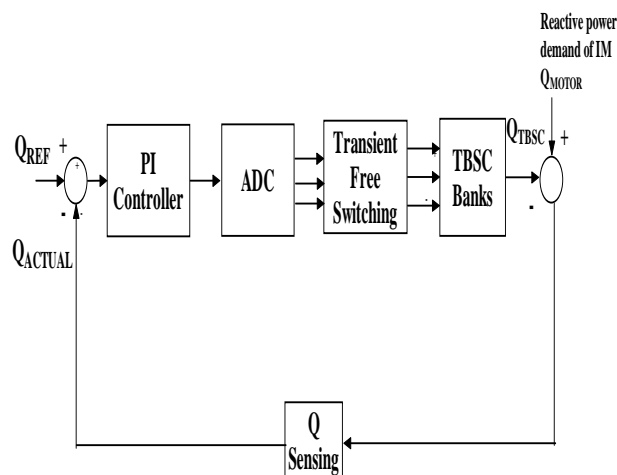


Fig. 2 TBSC closed loop operation

V. SIMULATION RESULTS
Data used in Simulation:-

- a. Source:-
Voltage $V = 400 \text{ V}$, $R_s = 0.0287\Omega$, $L_s = 0.20471\text{mH}$
- b. TBSC banks:-
Five TBSC banks are used in the simulation whose values are shown in Table I

TABLE I: TBSC values for Q, C and L

Sr. No.	Q (in KVAR)	C (in μF)	L (in mH)
1.	2.5	45	0.32
2.	5	90	0.16
3.	10	180	0.08
4.	20	360	0.04
5.	40	720	0.02

Continuously changing reactive power, Q_L is obtained by simulating three phase dynamic load. The nature of load variation is as shown in Fig.3. Minimum reactive power Q_{\min} , maximum reactive power Q_{\max} , and base reactive power Q_{Base} can be varied by changing the parameters of three phase dynamic load. In all simulations Q_{Ref} is set to zero since it is assumed that desired P.F. is unity at all times.

A TBSC Closed Loop Operation

Discrete PI controller with $K_p = 0.565$ & $K_I = 25$ is used. 5 bit ADC is used in simulation. Parameters of Three-phase dynamic load block are adjusted in such a way that Q_L varies continuously from $Q_{\min} = 2.5 \text{ KVAR}$ to $Q_{\max} = 77.5 \text{ KVAR}$ with base load $Q_{\text{Base}} = 40 \text{ KVAR}$. Waveforms of load reactive power Q_L , reactive power given by TBSC, $Q_{\text{comp. (TBSC)}}$ and actual reactive power Q_{Actual} at PCC are shown in Fig. 3. From simulation results it is seen that $Q_{\text{comp. (TBSC)}}$ closely follows Q_L shown in Fig.4, and actual reactive power Q_{Actual} at PCC is approximately zero at all times. The small error is due to the binary switching arrangement of TSCs. Current waveforms through all TBSC banks & source (of R phase) are shown in Fig.5 which are free from both harmonics and transients.

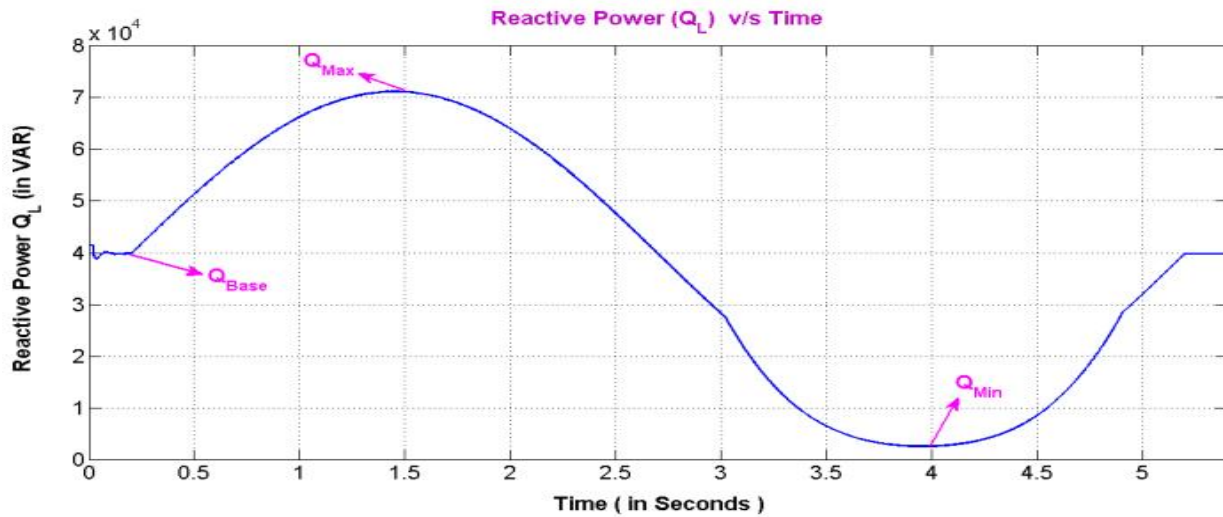


Fig.3 Simulation of three phase dynamic load

VI. CONCLUSION

A topology using a TBSC has been presented. The TSC bank step values are chosen in binary sequence weights to make the resolution small. Current flowing through TBSC as well as source is transient free. Harmonic content in source current is negligibly small. By coordinating the control of TBSC, it is possible to obtain fully stepless control of reactive power. Also one can operate the system at any desired power factor. Proposed topology can

compensate for rapid variation in reactive power on cycle to cycle basis. An attempt is made through this work to develop a scheme with thyristors to reduce the cost by avoiding IGBT's and IGCT's, technically sound with reliable performance during both steady state and transient conditions, suitable for rapidly changing / fluctuating loads such as arc furnaces, tractions loads, welding equipments etc., and self-regulating operations are practically both transient and harmonics free. The scheme developed is most suitable for highly nonlinear, fluctuating and harmonic

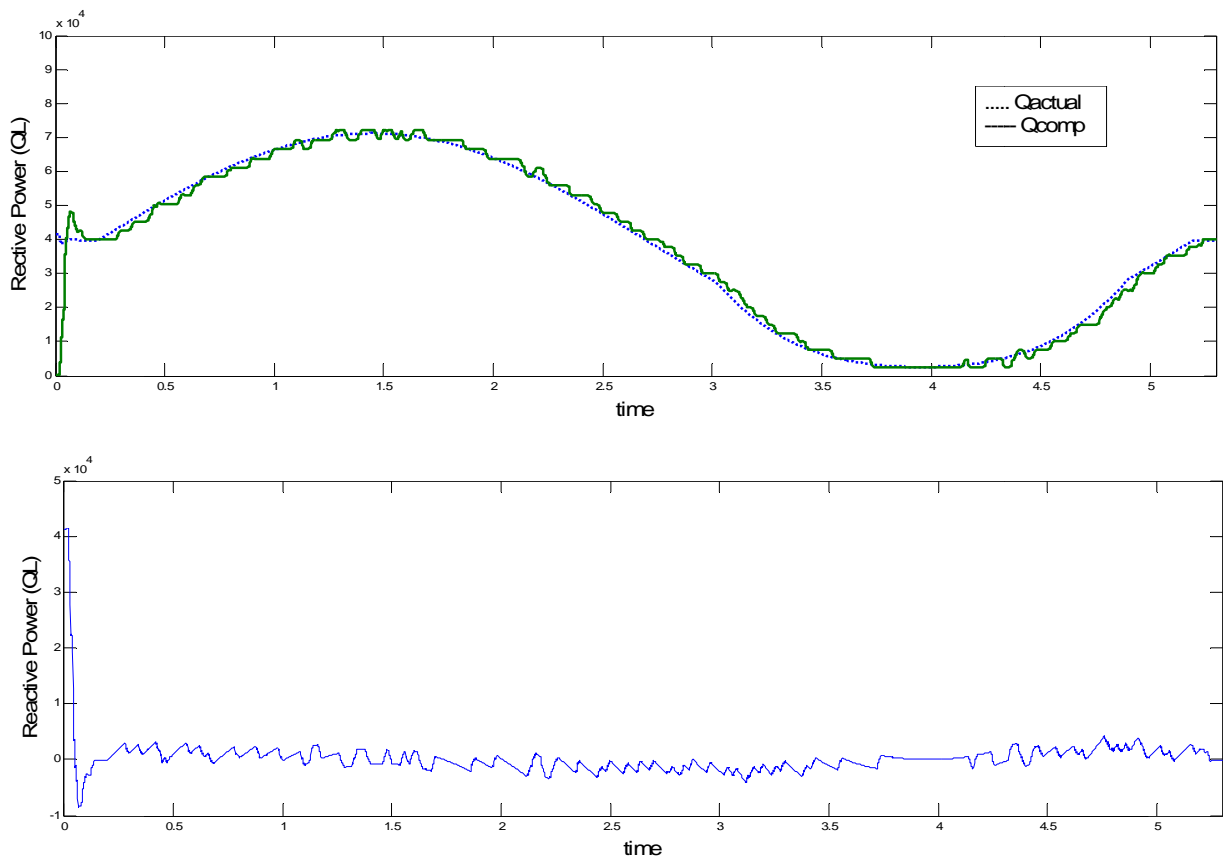


Fig. 4 Simulation results of TBSC closed loop operation

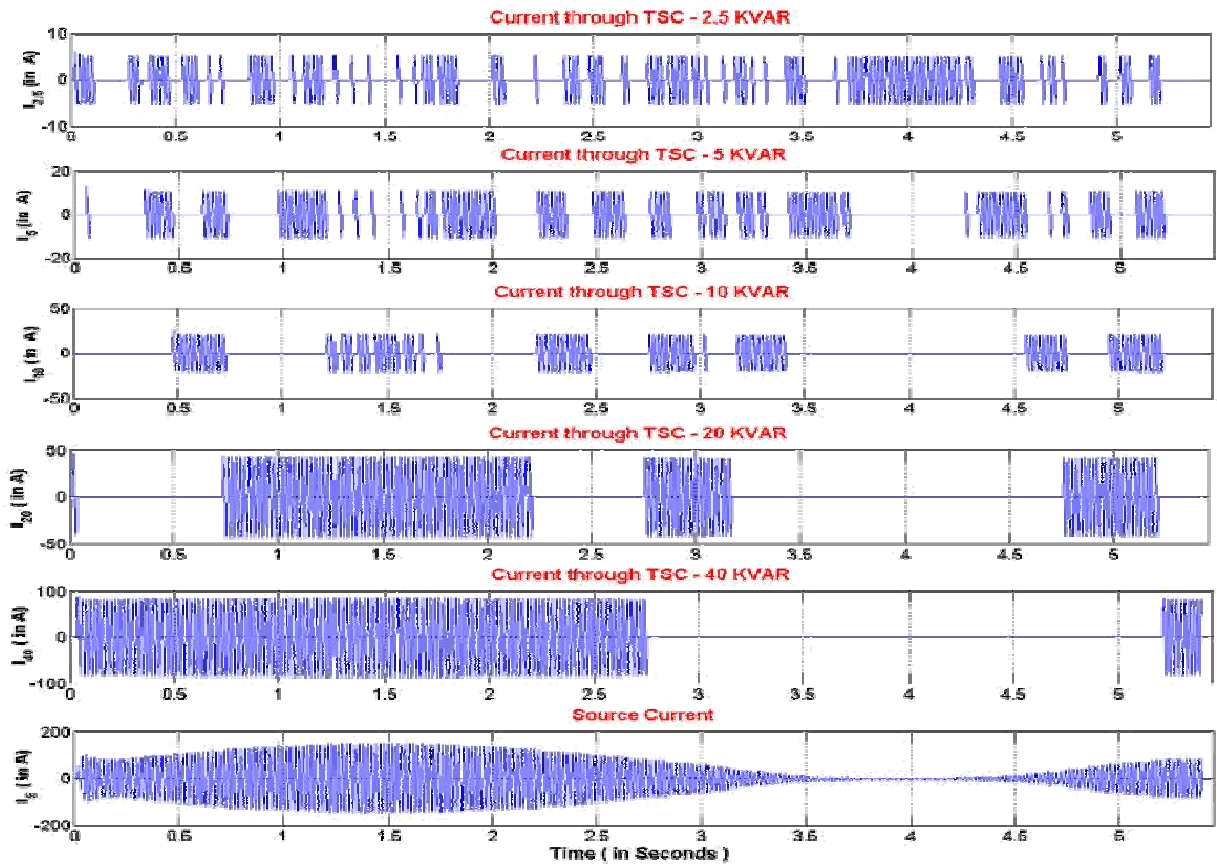


Fig. 5 Current Waveforms through all TBSC banks & Source (of R phase only)

generating loads. It gives following benefits.

- Maintaining the power factor at unity.
 - Minimum feeder current and loss reduction.
 - Improvement in distribution feeder efficiency
 - Improvement in the voltage at load end.
 - Relief in maximum demand and effective utilization of transformer capacity.
 - Saving in monthly bill due to reduction in penalty on account of poor power factor, and reduction in maximum demand charges.
 - Conservation of energy takes place
- It is possible to get stepless control of Q closely matching with load requirements.
- The combination offers greater flexibility in control

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