

Mode-Locking Intracavity Dynamics: Modeling Nonlinear Power and Energy Fluctuations

Brandon G. Bale* and J. Nathan Kutz†

Abstract—Modern high-power, pulsed lasers are driven by strong intracavity fluctuations. Critical in driving the intracavity dynamics is the nontrivial phase profiles generated and their periodic modification from either nonlinear mode-coupling, spectral filtering or dispersion management. Understanding the theoretical origins of the intracavity fluctuations helps guide the design, optimization and construction of efficient, high-power and high-energy pulsed laser cavities. Three specific mode-locking component are presented for enhancing laser energy: waveguide arrays, spectral filtering and dispersion management. Each component drives a strong intracavity dynamics that is captured through various modeling and analytic techniques.

Keywords: Modelocked lasers, waveguide arrays, spectral filtering

1 Introduction

High-power pulsed lasers are an increasingly important technological innovation as their conjectured and envisioned applications have grown significantly over the past decade. Indeed, this promising photonic technology has a wide number of applications ranging from military devices and precision medical surgery to optical interconnection networks [1]. Such technologies have placed a premium on the engineering and optimization of mode-locked laser cavities that produce stable and robust high-power pulses. Thus the technological demand for novel techniques for producing and stabilizing high-power pulses has pushed mode-locked lasers to the forefront of commercially viable, nonlinear photonic devices. The performance of the various mode-locking models are considered and optimized so as to produce high-power pulses in both the anomalous and normal dispersion regimes.

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The broader impact of mode-locked lasers has been limited due to restrictions on pulse energies, which is a consequence of the underlying cavity nonlinearities. Recently however, great effort and progress has been made experimentally to achieve mode-locked fiber lasers that produce high-energy, ultra-short pulses [5, 6]. A key parameter in achieving this aim is the cavity group velocity-dispersion (GVD). For anomalous GVD, ultra-short pulses can be easily obtained where the GVD balances the self-phase modulation (SPM) to produce soliton-like pulses that are nearly bandwidth-limited [1, 7]. The desire for higher energy pulses suggests consideration of cavities with segments of normal and anomalous GVD or with large and net normal GVD. These include the self-similar laser [8] and the chirped pulse oscillator (CPO) [9, 10]. In general, high-energy pulses can be generated, but it is necessary to compensate for the phase accumulated across the pulse [1, 7].

Recently, three new experimental configurations, operating in the non-soliton regime, have been developed for obtaining high pulse energies. First, robust and stable mode-locking can be achieved by using the nonlinear mode-coupling in a waveguide array as the intensity discrimination (saturable absorption) element in a laser cavity. Indeed, the spatial self-focusing behavior which arises from the nonlinear mode-coupling gives rise to ideal temporal pulse shaping and mode-locking [2, 3, 4]. Second, Chong *et al.* demonstrated a new class of high powered femtosecond fiber lasers, in which pulse-shaping is based on the spectral filtering of a highly-chirped pulse in the cavity [5, 6]. In contrast to soliton-like processes that dominate modern mode-locked lasers, these lasers depend strongly on dissipative processes as well as phase modulations to shape the pulse. Remarkably, no anomalous dispersion is required in the cavity, so this kind of laser is referred to as an all-normal dispersion (ANDi) laser. Third, self-similar (parabolic) pulse solutions have been recently observed experimentally [11, 12, 13] in laser cavities with a mean-zero GVD. In all these new lasers, the intracavity dynamics, generated either from the nonlinear mode-coupling, spectral filtering or dispersion management, plays a critical role in both stabilizing the mode-

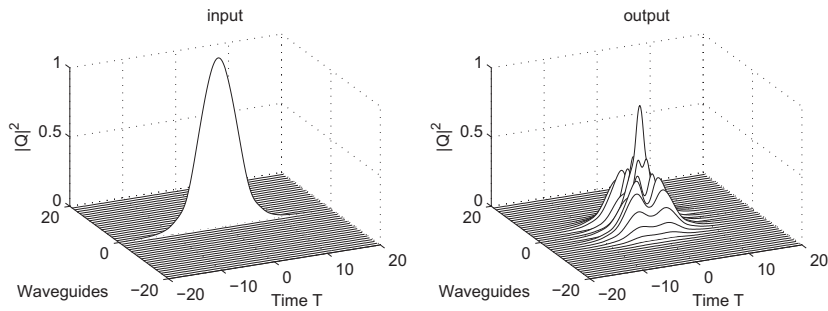


Figure 1: Input (A) and output (B) temporal power distribution in the WGA. At the input, energy is only launched in the center waveguide (A_0), while at the output the energy has spontaneously formed into the X-wave configuration involving about eleven guides. Only energy in the A_0 mode is preserved upon re-entry into the fiber section of the cavity.

locked pulse and producing high-energy output [14]. The aim of this manuscript is to highlight the modeling efforts required for quantifying the large intracavity fluctuations and to show how these fluctuations are key to generating novel, high-energy, mode-locked pulses. The analysis also provides a theoretical framework for optimizing the laser cavity performance and characterizing the global-attracting nature of the mode-locked solutions.

2 Intracavity Dynamics

We will consider three very different types of perturbations to the cavity: nonlinear mode-coupling, spectral filtering, and dispersion management. All three compensate for accumulated phase and produce high-energy pulses whose dynamics can be elegantly captured with asymptotic and perturbation methods.

2.1 X-wave formation in waveguide arrays

The theoretical model for the dynamic evolution of electromagnetic energy in the laser cavity with a waveguide array is composed of two components: the optical fiber and the nonlinear mode coupling element (NLMC) element, or waveguide array. The pulse propagation in a laser cavity is governed by the interaction of chromatic dispersion, self-phase modulation, linear attenuation, and bandwidth limited gain. The propagation is given by [1]

$$i \frac{\partial Q}{\partial Z} + \frac{1}{2} \frac{\partial^2 Q}{\partial T^2} + |Q|^2 Q + i\gamma Q - ig(Z) \left(1 + \tau \frac{\partial^2}{\partial T^2} \right) Q = 0, \quad (1)$$

where

$$g(Z) = \frac{2g_0}{1 + \|Q\|^2/e_0}, \quad (2)$$

Q represents the electric field envelope normalized by the peak field power $|Q_0|^2$, and $\|Q\|^2 = \int_{-\infty}^{\infty} |Q|^2 dT$. Here the variable T represents the physical time in the

rest frame of the pulse normalized by $T_0/1.76$ where $T_0=200$ fs is the typical full-width at half-maximum of the pulse. The variable Z is scaled on the dispersion length $Z_0 = (2\pi c)/(\lambda_0^2 \bar{D})(T_0/1.76)^2$ corresponding to an average cavity dispersion $\bar{D} \approx 12$ ps/km-nm. This gives the one-soliton peak field power $|Q_0|^2 = \lambda_0 A_{\text{eff}}/(4\pi n_2 Z_0)$. Further, $n_2 = 2.6 \times 10^{-16}$ cm²/W is the nonlinear coefficient in the fiber, $A_{\text{eff}} = 60$ μm^2 is the effective cross-sectional area, $\lambda_0 = 1.55$ μm is the free-space wavelength, c is the speed of light, and $\gamma = \Gamma Z_0$ ($\Gamma = 0.2$ dB/km) is the fiber loss. The bandwidth limited gain in the fiber is incorporated through the dimensionless parameters g and $\tau = (1/\Omega^2)(1.76/T_0)^2$. For a gain bandwidth which can vary from $\Delta\lambda=20-40$ nm, $\Omega = (2\pi c/\lambda_0^2)\Delta\lambda$ so that $\tau \approx 0.08-0.32$. The parameter τ controls the spectral gain bandwidth of the mode-locking process, limiting the pulse width.

It should be noted that a solid-state configuration can also be used to construct the laser cavity. As with optical fibers, the solid state components of the laser can be engineered to control the various physical effects associated with (1). Given the robustness of the mode-locking observed, the theoretical and computational predictions considered here are expected to hold for the solid-state setup. Indeed, the NLMC acts as an ideal saturable absorber and even large perturbations in the cavity parameters (e.g. dispersion-management, attenuation, polarization rotation, higher-order dispersion, etc.) do not destabilize the mode-locking.

The leading-order equations governing the nearest-neighbor coupling of electromagnetic energy in the waveguide array is given by [15, 16, 17, 18, 19]

$$i \frac{dA_n}{d\xi} + C(A_{n-1} + A_{n+1}) + \beta |A_n|^2 A_n = 0, \quad (3)$$

where A_n represents the normalized amplitude in the

n^{th} waveguide ($n = -N, \dots, -1, 0, 1, \dots, N$ and there are $2N + 1$ waveguides). The peak field power is again normalized by $|Q_0|^2$ as in Eq. (1). Here, the variable ξ is scaled by the typical waveguide array length [17] of $Z_0^* = 6$ mm. This gives $C = cZ_0^*$ and $\beta = (\gamma^* Z_0^* / \gamma Z_0)$. To make connection with a physically realizable waveguide array [18], we take the linear coupling coefficient to be $c = 0.82 \text{ mm}^{-1}$ and the nonlinear self-phase modulation parameter to be $\gamma^* = 3.6 \text{ m}^{-1} \text{ W}^{-1}$. Note that for the fiber parameters considered, the nonlinear fiber parameter is $\gamma = 2\pi n_2 / (\lambda_0 A_{\text{eff}}) = 0.0017 \text{ m}^{-1} \text{ W}^{-1}$. These physical values give $C = 4.92$ and $\beta = 15.1$. The periodic waveguide spacing is fixed so that the nearest-neighbor linear coupling dominates the interaction between waveguides. Over the distances of propagation considered here (e.g. $Z_0^* = 6$ mm), dispersion and linear attenuation can be ignored in the waveguide array.

The values of the linear and nonlinear coupling parameters are based upon recent experiment [17]. For alternative NLMC devices such as dual-core fibers or fiber arrays, these parameters can be changed substantially. Further, in the dual-core fiber case, only two waveguides are coupled together so that the $n = 0$ and $n = 1$ are the only two modes present in the dynamic interaction. For fiber arrays, the hexagonal structure of the waveguides couples an individual waveguide to six of its nearest neighbors. Regardless of these model modifications, the basic NLMC dynamics remains qualitatively the same.

To illustrate the pulse shaping properties and the spontaneous formation of an X-wave structure in the normal GVD regime [20], we integrate numerically the proposed infinite-dimensional map by alternating Eqs. (1) and (2) for a length L_f and Eqs. (3) for a length L_a . Thus Q of Eq. (1) becomes A_0 in Eq. (3) when entering or leaving the waveguide array. Importantly, upon exiting the WGA, the system is strongly perturbed since the energy from all the neighboring channels (A_i where $i = \pm 1, 2, 3, \dots$) are expelled from the laser cavity. Nevertheless, we observe the formation of a stable mode-locked pulse which shows the field A_0 at the output. The white-noise is quickly reshaped (over 10 round trips) into the mode-locking pulse of interest. Thus the mode-locking pulse acts as a *global attractor* to the laser cavity system. The simulation further implies that the mode-locking behavior is stable in the sense of Floquet since it is a periodic solution in the cavity. The spectral shape clearly indicates that the mode-locking pulse is highly chirped, in analogy to what is found for 1D (no spatial dynamics) solutions of the master mode-locking equations in the normal GVD regime [1].

The overall electromagnetic field actually experiences a strong spatio-temporal reshaping per cavity round trip

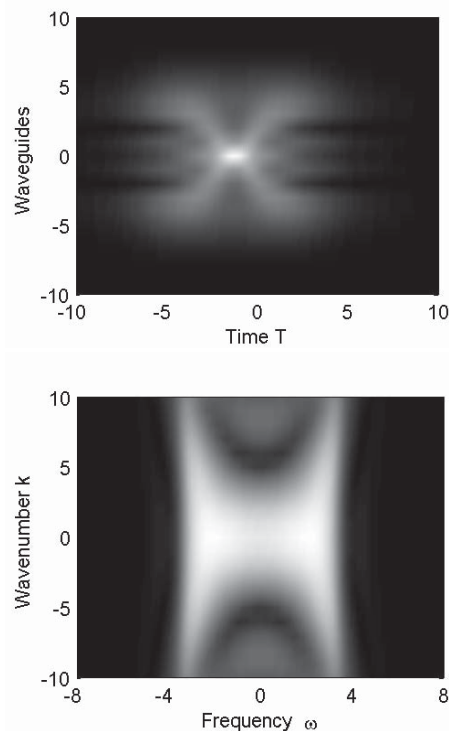


Figure 2: Time-domain profiles and its two-dimensional Fourier transform at the output (B) in the WGA after steady-state mode-locking has been achieved. The X-wave structure is clearly seen in the topographical plot (top) of the output time-domain profiles of Fig. 1. Further, the expected wavenumber versus frequency dependence in the X-wave is shown in the Fourier domain (bottom).

that involves stable coupling of a significant portion of the incoming WGA power to neighboring waveguides with nontrivial timing. The input and output time-domain intensities in all the waveguides, once nonlinear mode-locking has been achieved are displayed in Fig. 1. As shown, the interplay of accumulated GVD, discrete diffraction, and nonlinearity drives the field into a self-organized nonlinear X-waves, whose main signature is a central peak accompanied by pulse splitting occurring in the external channels. To show more clearly the X-shape of the mode-locking wave-packet generated at the output (B) of the waveguide array, Fig. 2 depicts a topographical plot of the time-domain (top) of all the waveguides. The distinctive X-wave structure is clearly evident. To lend further evidence to the existence of the X-wave structure, we plot the 2D Fourier transform of the time-domain. The right panel of Fig. 2 demonstrates that the spectrum is also X-shaped, as expected for X-waves [21, 22].

To further characterize the mode-locking X-wave dynamics, Fig. 3 illustrates the mode-locking to the global attractor in the neighboring waveguides A_1 , A_2 and A_3 . Once again, generic white-noise initial data quickly self-organize into the steady-state mode-locking pattern. Note the characteristic pulse splitting (dip in the power) in the neighboring waveguides. This shows, in part, the generated X-wave structure. The final panel in Fig. 3 gives the energy ($\int_{-\infty}^{\infty} |A_j|^2 dT$) in each of the waveguides and shows that a significant portion (more than 50%) of the electromagnetic energy has coupled to the neighboring waveguides. This is in sharp contrast to mode-locking with anomalous GVD for which less than 6% is lost to the neighboring waveguides [4] and no stable X-waves are formed. The significant loss of energy in the cavity to the neighboring waveguides is compensated by the gain section and shows that the laser cavity is a strongly damped-driven system.

2.2 Spectral Filtering

The evolution of electromagnetic energy in the laser cavity is subject to a number of physical components: dispersion elements, bandwidth-limited gain components, and saturable absorption (intensity-discrimination) elements. These components are responsible for generating, among other things, intra-cavity chromatic dispersion, self-phase modulation, attenuation, and gain saturation. Haus proposed that these different elements could be averaged together into a single Ginzburg-Landau type evolution equation: the master mode-locking model [23]. Due to stability considerations, the master equation is often augmented by a quintic saturation term which prevents blow-up of the solution. Thus the cubic-quintic Ginzburg-Landau equation (CQGLE) incorporates the laser cavity's intensity discrimination in a phenomenological way. The governing evolution is then given by

$$i \frac{\partial u}{\partial z} + \frac{D}{2} \frac{\partial^2 u}{\partial t^2} + (1+i\beta)|u|^2 u + i\sigma|u|^4 u + i\delta u - ig(z) \left(1 + \tau \frac{\partial^2}{\partial t^2}\right) u = 0, \quad (4)$$

where the saturated gain behavior is given by [1, 7]

$$g(z) = \frac{2g_0}{1 + \|u\|^2/e_0}. \quad (5)$$

Here u is the electric field envelope, z is the propagation distance, and t is the retarded time. The energy of the pulse is given by $\|u\| = \int_{-\infty}^{\infty} |u|^2 dt$, and β and σ measures the strength of the cubic and quintic saturable absorber terms respectively. The parameters δ , g_0 and e_0 measure the cavity attenuation, the amplifier gain strength, and cavity saturation energy respectively.

The governing equation (4) is a partial differential equation modeling the spatial-temporal evolution of electromagnetic energy in the laser cavity. The variational method can be used to capture the intra-cavity pulse dynamics. The literature regarding variational reductions [24] in nonlinear Schrödinger type systems is vast, especially given its applicability in optical transmission systems. To fully capture the varying phase profiles which have been observed in the ANDi laser cavity [5, 6], we assume a solution-based mode-locking ansatz form

$$u(z, t) = \frac{\eta(z)}{\sqrt{B(z) + \cosh(\eta(z)t)}} e^{-i\Psi(z, t)} \quad (6)$$

with $\Psi(z, t) = A(z) \ln(B(z) + \cosh(\eta(z)t)) + \varphi(z)$. The specific form of the phase profile Ψ is essential to capture the different spectral profiles observed in the ANDi laser [5, 6]. The evolution of the ansatz parameters as a function of propagation distance [24] is then found to satisfy the ordinary differential equations

$$D\mathbf{x} = \mathbf{g} \quad (7)$$

where $\mathbf{x} = [\eta_z, B_z, A_z, \varphi_z]^T$, $\mathbf{g} = [g_1, g_2, g_3, g_4]^T$, and

$$D = \begin{bmatrix} H & \eta H' & 0 & 0 \\ (H-G) & -\eta(G'+H') & 0 & 0 \\ 0 & -AH' & \frac{1}{2}(G-H) & -H \\ AH' & 0 & \frac{1}{2}\eta(G'+H') & -\eta H' \end{bmatrix}. \quad (8)$$

The components in the vector \mathbf{g} include the terms from dispersion and self-phase modulation, as well as the gain and loss perturbations. They are given by

$$g_1 = 2\eta(g-\delta)H - 2\epsilon\eta^3 H' + \sigma\eta^5 H'' - \frac{1}{2}\tau g\eta^3(A^2+1)R \quad (9a)$$

$$g_2 = \frac{D}{2}\eta^3 AR - 2\eta(g-\delta)G - 2\epsilon\eta^3 S - 2\sigma\eta^5 Z + \frac{1}{2}\tau g\eta^3 [3W - 2Y - WA^2] \quad (9b)$$

$$g_3 = \frac{3D\eta^2}{4}(1+A^2)R + \frac{3\eta^2 H'}{2} - 2A(g-\delta)H + \epsilon\eta^2 AH' - \frac{\sigma\eta^4 AH''}{3} + \frac{\tau g\eta^2 A}{2}(1+A^2)Q \quad (9c)$$

$$g_4 = \frac{D}{4}\eta^3(1+A^2)R' + \frac{\eta^3 H''}{2} - 2\eta A(g-\delta)H' - \epsilon\eta^3 AH'' + \frac{\sigma\eta^5 AH'''}{3} - \frac{\tau g\eta^3 A}{12}(1+A^2)R', \quad (9d)$$

where all primes denote differentiation with respect to the parameter B , and the parameters H, G, Q, R, S, W, Y and Z are B -dependent integrals given by

$$H = \int \frac{dt}{\Theta}, \quad G = \int \frac{\ln \Theta dt}{\Theta}, \quad Q = \int \frac{t \sinh^3 t dt}{\Theta^4},$$

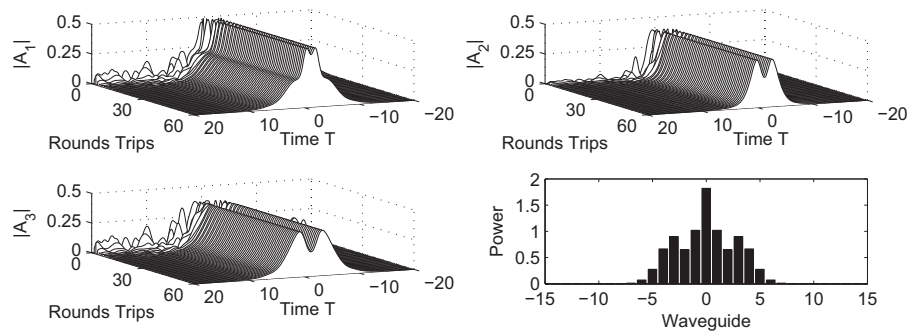


Figure 3: Evolution to the steady-state output (B) in the neighboring waveguides A_1 , A_2 , and A_3 . The bottom right graph is a bar graph of the steady-state distribution of energy ($\int_{-\infty}^{\infty} |A_j|^2 dT$) in the waveguides. The symmetry about the center waveguide results from the initial condition being applied only in this waveguide. Note the significant re-distribution of energy in the waveguides.

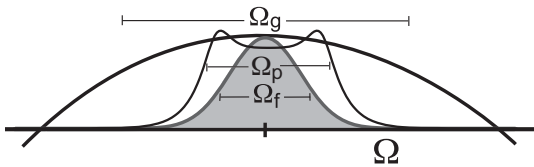


Figure 4: The experimental laser cavity configuration includes an amplifier with parabolic gain bandwidth Ω_g and a Gaussian spectral filter with bandwidth Ω_f . A typical pulse solution with spectral bandwidth Ω_p is also shown. Note that the key parameter $\Gamma = \Omega_f/\Omega_p$.

$$R = \int \frac{\sinh^2 t dt}{\Theta^2}, S = \int \frac{\ln \Theta dt}{\Theta^2}, W = \int \frac{\sinh^2 t \ln \Theta dt}{\Theta^3},$$

$$Y = \int \frac{\cosh t \ln \Theta dt}{\Theta^2}, Z = \int \frac{\ln \Theta dt}{\Theta^3} \quad (10)$$

with $\Theta = B + \cosh t$ and all integrations range over $t \in [-\infty, \infty]$.

Despite the complicated structure of the equations, the dynamics are quite easy to characterize. The phase variable φ can easily be eliminated from the system (7) resulting in a 3×3 system that can be analyzed in the phase plane. For different parameter regimes, the dynamics exhibits a stable node, a stable spiral node and a limit cycle in the η, B and A phase plane. The location of the fixed point as well as its stability depend on the parameters in the equations. The key contribution to pulse shaping in the ANDi lasers arises from the spectral filter. Although the fixed points of the reduced model have the correct temporal and spectral profiles seen in the ANDi laser, it fails to capture the round trip cavity dynamics [5, 6]. To capture the intra-cavity pulse fluctuations we must consider the operation of the spectral filter. The spectral

filter can be assumed to be a Gaussian function with full width half maximum (FWHM) Ω_f , and will typically fall under the gain bandwidth, as shown in Fig. 4. The ratio $\Gamma = \Omega_f/\Omega_p$, where Ω_p is the FWHM of the pulse bandwidth, determines how significant the filtering action is. For example, if $\Gamma \gg 1$, then the filter will have no effect on the pulse, however if $0 < \Gamma < 1$ then the filter will modify the pulse solution in some way. The typical evolution of the electromagnetic energy with all laser cavity components is demonstrated in Fig. 5. Our goal is provide a qualitatively and quantitatively accurate description of these dynamics with the variational reduction.

To observe the spectral profile evolution per round trip in the laser cavity, the filter action cannot be averaged into Eq. (4) and must be considered as a discrete forcing on the governing equations. To obtain an understanding of the mechanism of the filter, we consider its effects in the context of the reduced model. For bandwidth ratios $0 \ll \Gamma < 1$, multiplying the spectrum of (6) by a Gaussian filter results in a similar pulse form with modified parameters. Thus we are able to assume that the filter acts only on the fixed point (η_0, B_0, A_0) of the dynamical system (7), modifying the fixed point in some way, i.e. $(\eta_0, B_0, A_0) \rightarrow (\eta_f, B_f, A_f)$ where the new values are computed numerically after filtering via a least-square fitting. The accurate spectral and temporal fit between the post-filtered pulse and the pulse solution (6) with modified parameters clearly illustrates that the application of the spectral filter on the fixed point solution effectively changes the pulse parameters. Combining the reduced model, which is based on averaged evolution equations, with the essential discrete element in the laser, the spectral filter, we obtain a graphical interpretation of the intra-cavity dynamics of the ANDi laser since the filter acts as a periodic forcing (per round trip) on the governing equations that modifies the fixed point solution

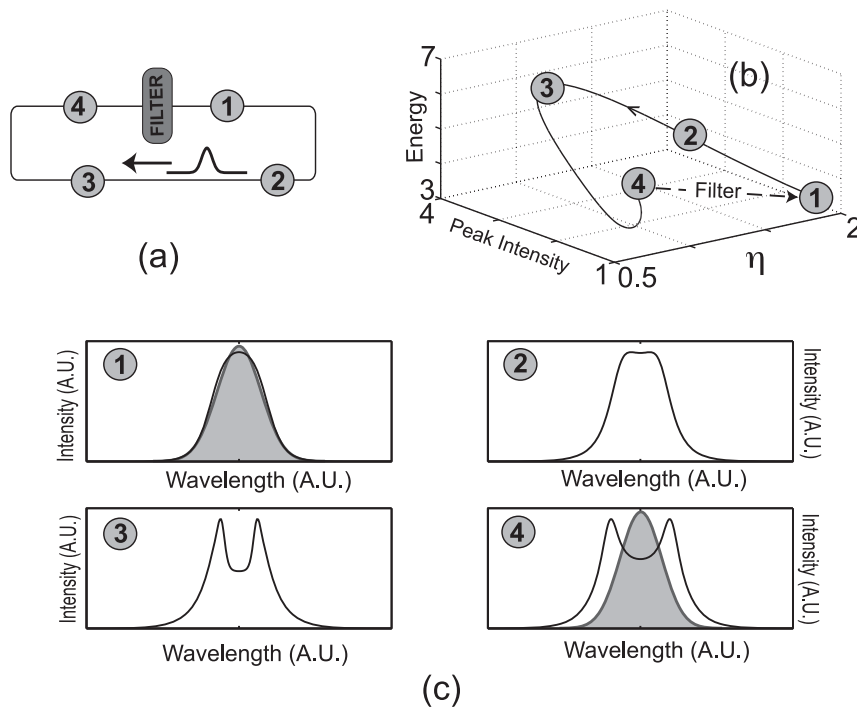


Figure 6: (a) Illustration of the laser cavity with discrete filter and four labeled positions in the cavity. (b) The intra-cavity mode-locked evolution in the experimentally relevant variables along with the action of the spectral filtering (dotted line). (c) The output spectral profiles at the labeled intra-cavity positions of (a) and (b). This prototypical pulse evolution is characteristic of the all-normal dispersion fiber laser [6]. Note that high energy, high peak amplitude pulses can be obtained if the output coupler is placed at position 3.

parameters (η_0, B_0, A_0) . We consider a laser configuration with the parameters $g_0 = 3, \delta = 1, \tau = 0.2, D = -0.4, \epsilon = 0.5$, and $\sigma = -0.1$ corresponding to a stable node at $(\eta_0, B_0, A_0) = (1, -0.5, 3.3)$.

By examining the evolution along flow lines we can understand the dynamics of the ANDi laser. Figure 6 shows an example of the laser dynamics with a filter bandwidth ratio $\Gamma = 0.5$. Figure 6(a) shows the laser configuration with the spectral filter as the primary discrete element. Figure 6(b) illustrates the phase line (whose initial condition is specified by the spectral filter width) in a relevant phase plane whose phase variables are the pulse duration (η) , peak amplitude $(\eta/(1+B))$, and pulse energy $\eta F(B)$. Figure 6(c) shows the spectral profiles at the various positions labeled in the laser set-up and phase plane. The fixed point is denoted by “4”, where the pulse directly after filtering is denoted by the “1” position. The periodic application of the filter (once per round trip) actively controls the parameters of the mode-locked pulse, changing the pulse solution parameters in (6) from the fixed point “1” to position “4”. Further, along the flow line the dynamic pulse evolution contains different spec-

tral profiles that have been observed experimentally in the ANDi laser cavity [5, 6]. Note that the periodic orbit acts as a globally attracting state of the system, producing large intracavity fluctuations per round trip of the cavity. The optimal energy and peak power output can be extracted from the laser cavity at position “3” as is graphically demonstrated.

2.3 Self-Similar Mode-locking

In contrast to spectral filtering, we can also achieve the necessary phase compensation by applying a dispersion map to the laser cavity. This in turn will generate large intracavity fluctuations. In this case, the parameter D in (4) is dependent upon z . We investigate (4) when the dispersion length Z_0 is much longer than the typical period P of the dispersion map, so that

$$\epsilon = P/Z_0 \ll 1 \quad (11)$$

and the dispersion fluctuations occur on a rapid scale. The period P is simply determined by the physical length of the laser cavity while the dispersion length is related to the pulse width of the mode-locked pulses. Specifically, the dispersion length is the length it takes for the

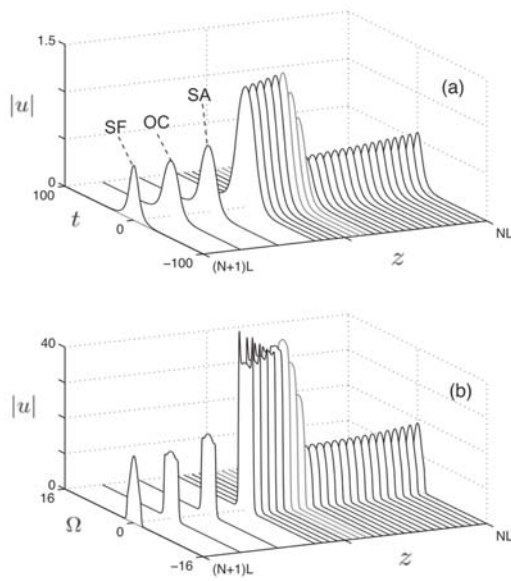


Figure 5: Typical temporal (a) and spectral (b) solutions from numerical simulation of the CQGLE equation with spectral filtering for an all-normal dispersion laser. Note that the saturable absorber (SA), output coupler (OC), and spectral filter (SF) are applied in series resulting in the last three pulses in the map. Gray shade corresponds to the gain segment.

full-width, half-maximum pulse width to double in the absence of nonlinearities. For convenience and simplicity, we let

$$D = d(z/\epsilon) = \cos(2\pi z/\epsilon). \quad (12)$$

Note that although the results apply to a general $d(z)$, it will prove helpful to consider the particular case here of a simple sinusoidal dispersion map.

Simulations suggest that the dispersion fluctuations must occur on a rapid-scale in order for the parabolic states to persist. Such a clear scale separation between the dispersion map period and the fundamental dispersion and nonlinearity scale suggests the application of a multi-scale transformation technique. The transformation procedure considered relies on the Green's function of the linear part of the left hand side of (4) since it accounts explicitly for the dispersion fluctuations. Using Fourier transforms, it is easy to calculate that the Green's function for the linear Schrödinger equation [25]

$$i \mathbf{G}_z + \frac{1}{2} d(z/\epsilon) \mathbf{G}_{tt} = 0, \quad (13)$$

with $\mathbf{G}(t, t', 0) = \delta(t - t')$ is given by

$$\mathbf{G}(t, t', z) = \frac{\exp(i\pi/4)}{\sqrt{4\pi\mu(z)}} \exp\left(\frac{-i(t-t')^2}{4\mu(z)}\right). \quad (14)$$

Here $2\mu(z) = \int_0^z d(s)ds \sim O(\epsilon)$ is the accumulated dispersion for a rapidly-varying, mean-zero map.

The transformation is performed by introducing the new function $A(t, z)$ defined by

$$A(t, z) = \int \mathbf{G}^\dagger(t, t', z) u(t', z) dt'. \quad (15)$$

The evolution equation for A can be found by using the adjoint relation $u(t, z) = \int \mathbf{G}(\xi, t, z) A(\xi, z) d\xi$. Plugging this into the governing equation (4), making use of (13), then multiplying by the adjoint $\mathbf{G}^\dagger(\xi, t, z)$ and integrating with respect to ξ gives an exact transformation. At this point no approximations have been made – the transformation from u to A is simply a linear change of variables. Since $\mu \sim \epsilon \ll 1$, the integrals can be approximated using stationary-phase asymptotics [25]. Expanding the integrals about the stationary phase points gives an approximate evolution for A in terms as a series expansion in $\mu \sim \epsilon \ll 1$. Further, we assume that δ , τ , μ , β , and σ are small parameters thus allowing us to neglect higher order terms with $\mu\delta$, $\mu\beta$, etc., products.

The effective equation can be put into a more transparent form with the amplitude-phase decomposition $A(t, z) = \sqrt{\rho(t, z)} \exp(i\Theta(t, z))$ so that

$$\rho_z = \mu(z)(\rho^2)_{tt} + 2\rho(\delta - \beta\rho - \sigma\rho^2) + \tau\left(\rho_{tt} - \frac{\rho_t^2}{2\rho} - 2\rho\Theta_t^2\right) \quad (16a)$$

$$\Theta_z = -\rho - 2\mu(z)\rho\Theta_{tt} + \tau\left(\Theta_{tt} + \frac{1}{\rho}\rho_t\Theta_t\right). \quad (16b)$$

A key observation is that for $\mu > 0$ the phase equation (16b) is ill-posed whereas for $\mu < 0$ the amplitude equation (16a) is ill-posed. This problem is an artifact of the averaging process and can be treated via regularization or by including higher order correction terms [25]. In contrast to other averaging techniques used on dispersion managed systems, we emphasize that the averaging technique used here retains the critical dependence of the parameter μ on z . This plays a key role in the stabilization of the parabolic state. Indeed, if the $\mu(z)$ parameter is averaged out to be a constant, the theory fails to correctly capture the breathing nature of the solutions. Specifically, the profile undergoes typical self-similar broadening until the expansion formally breaks down at $z \sim 1/\sqrt{\epsilon}$ [25].

In the limit where the dissipative perturbations on the right hand side of (4) are small in comparison with the dispersion map, i.e. $(\delta, \beta, \sigma, \tau) \ll \epsilon < 1$, the leading order amplitude equation is governed by the porous media equation

$$\rho_z = \mu(z)(\rho^2)_{tt}. \quad (17)$$

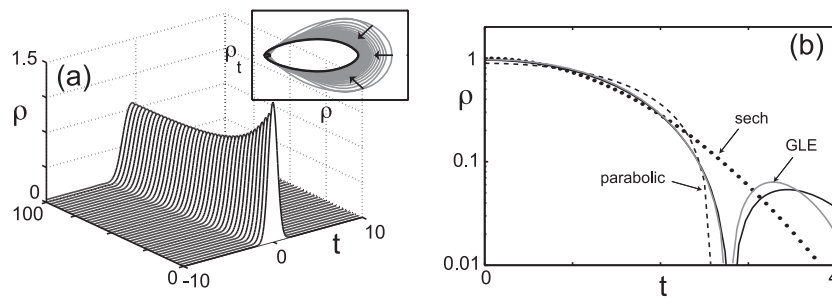


Figure 7: Attracting dynamics of the solution (a) and its phase-plane (inset) obtained from numerical simulation of the amplitude equation (19) from a Gaussian initial condition with $\delta = 0$, $\beta = \sigma = 0.1$, and $\epsilon = 0.5$. The output is shown at the beginning of each dispersion map. (b) Comparison of the parabolic solution from solving (19) numerically (solid black) with the solution from the full governing Ginzburg-Landau equation (4) (solid grey), a quadratic Barenblatt profile (dashed) and hyperbolic secant pulse (dots). The tail structure is also exhibited in experiments [11].

The porous media equation has the Barenblatt similarity solution

$$|u|^2 \approx \rho(t, z) \sim \frac{1}{12(\gamma + z_*)^{1/3}} \left[a_*^2 - \left(\frac{t - t_*}{(\gamma + z_*)^{1/3}} \right)^2 \right]_+ \quad (18)$$

where $\gamma = \gamma(z) = 2 \int_0^z \mu(s) ds$ and $f_+ = \max(f, 0)$ so that the subscript $+$ indicates that the function is either zero or positive in (18). The solution is characterized by the three parameters (a_*, t_*, z_*) which represent the mass, center position, and pulse-width of the solution respectively. Note that $u \approx A$ when $\epsilon \ll 1$ [25]. Here, to first order in $\mu \sim \epsilon$, the evolution equation for the amplitude decouples from the equation for the phase. We emphasize that the breathing dynamics results from the periodic fluctuations in the integral of the cumulative dispersion $\gamma(z)$. Indeed, the averaging technique used here retains the oscillatory nature of the dispersion map in the form of a z -dependent oscillatory coefficient in Eqs. (18). This oscillatory variation suppresses the structure from undergoing its usual self-similar broadening and allows for stable self-similar breathers.

Although the Barenblatt solution (18) captures the fundamental self-similar structure, it is not the attracting state of the underlying system. This is expected since we have neglected the dissipative terms needed to create an attractor. Further, the Barenblatt solution has unphysical discontinuous derivatives at its edges. So although insightful, it is a mathematical idealization that is physically unrealizable. In many applications, spectral filtering is much weaker than other dissipative terms, i.e. $\tau \ll (\delta, \beta, \sigma, \mu)$. In this case, the amplitude equation

$$\rho_z = \mu(z)(\rho^2)_{tt} + 2\rho(\delta - \beta\rho - \sigma\rho^2), \quad (19)$$

is still decoupled from the phase equation. Although ex-

act solutions to (19) are not attainable, this equation sheds light on why parabolic states persist in this system. Specifically, for small values of the parameters δ , β and σ , equation (19) is perturbatively close to (17). Likewise, the solutions of the two equations should also be perturbatively close so that the leading order behavior of (19) inherits the self-similar Barenblatt structure of (18). Note that this implies that (19) is not strictly self-similar as certain symmetries associated with (17) are broken. Regardless, the inclusion of dissipative terms allows for an attracting parabolic breathers to exist for a wide range of parameter space. Further, numerical simulations suggest the parabolic states are robust to a variety of perturbations including white-noise fluctuations.

Figure 7 shows the numerical simulation of (19) from initial amplitude $\rho(t, 0) = \sqrt{2} \exp[-t^2]$. The output point in the Poincaré map is taken to be at the beginning of each map period. Figure 7(a) shows that the initial Gaussian structure quickly settles to a steady state solution in the Poincaré map. In contrast to the Barenblatt solution, the output pulse profile here has finite derivatives at its edges. The inset of Fig. 7(a) plots the corresponding (ρ, ρ_t) phase plane and shows that there is indeed an attracting homoclinic orbit (solid line) which represents the steady state solution. To show that this attracting state has a parabolic profile, the output pulse (once settled to the parabolic breather), along with a Barenblatt quadratic (dashed) and hyperbolic secant (dotted) fit is plotted in Fig. 7(b). In addition, the numerical solution for the Ginzburg-Landau equation (4) with parameters $\tau = \delta = 0$, $-\beta = \sigma = 0.1$, and $\epsilon = 0.5$ is included (solid grey). This shows that the solutions to (4) and (19) are perturbatively close as expected. Further, there is the remarkable agreement between the solution profile of (19) and experiments [11]. Unlike the Barenblatt so-

lution, the parabolic solution to (19) correctly captures the tail structure observed in experiments [11]. Further, the solution is a global attractor of the system.

3 Conclusions

In conclusion, we have shown that the consideration of the large intracavity dynamics generated from either nonlinear mode-coupling (waveguide arrays), spectral filtering or mean-zero, dispersion management leads to non-trivial, periodic mode-locked states that act as global attractors to the laser. For nonlinear mode-coupling, the spontaneous formation of X-wave structures is demonstrated. In the all-normal dispersion fiber laser with filtering, we characterized these behaviors with a reduced model which is based on an averaged CQGLE equation. A key contribution to pulse shaping in these lasers arises from the spectral filter, which converts large frequency chirp to self-amplitude modulation. The variational method used here provides a geometrical interpretation that completely describes the intra-cavity dynamics. The resulting intra-cavity temporal and spectral profiles are in good agreement with experimental results. Thus the laser can be engineered to take advantage of the intra-cavity pulse dynamics by placing the output coupler at positions where the pulse has the desired output profile. When considering a rapidly-varying, mean-zero dispersion, the intracavity evolution dynamics results in a perturbed version of the nonlinear (porous media) diffusion equation with mean-zero diffusion coefficient. The dissipative contributions in the GL equation make the parabolic structure an attracting state of the system. Thus the two driving mechanisms of parabolic propagation are the mean-zero dispersion map which generates self-similarity and dissipation which makes the self-similar structure an attractor. The combination of the two phenomena result in the formation of the parabolic breathers that have been observed experimentally [11].

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