Improved NSGA-III Algorithm and BP Fuel-cost Prediction Network for Many-objective Optimal Power Flow Problems

Jie Qian, Hongyu Long^{*}, Yi Long, and Chenxu Zhao

Abstract—To effectively handle the many-objective optimal power flow (MOOPF) problems considering the simultaneous reduction of power loss, emission and fuel cost, an improved NSGA-III (INSGA-III) algorithm is put forward in this paper. In detail, the proposed INSGA-III algorithm adopts the competitive solutions preliminarily optimized by traditional NSGA-III method as the initial population and integrates the novel adaptive dominant (NAD) strategy. Comparing with the original NSGA-III algorithm, INSGA-III obtains the more preferable Pareto front (PF) with uniform distribution. More significantly, an entirely new BP fuel-cost prediction network is proposed to explore the potential elite power flow (EPL) solutions. These EPL solutions determined around the best compromise solution (BCS) of INSGA-III algorithm provide decision-makers with more and better scheduling schemes. The effectiveness and superiorities of proposed INSGA-III algorithm and BP fuel-cost prediction model are verified by both dual-objective and triple-objective MOOPF simulation experiments. In general, this paper presents an innovative way to solve the complex engineering problems by computer technologies represented by intelligent algorithms and neural networks.

Index Terms—Improved NSGA-III algorithm, Manyobjective optimal power flow, Adaptive dominant strategy, BP fuel-cost prediction network, Computer technologies

I. INTRODUCTION

IN order to realize the economic and safe operation of power systems, the high-quality dispatching schemes which can reduce the fuel cost, active power loss and emission are needed. At present, the optimal power flow (OPF) problems considering only single objective cannot satisfy the various needs of users. Therefore, more scholars focus on the many-objective OPF (MOOPF) problems which aim to achieve the simultaneous reduction of two or three goals [1-4].

To solve MOOPF problems is actually to seek a feasible

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Chenxu Zhao is a senior engineer of Inner Mongolia Power (Group) Co., Ltd, Inner Mongolia Power Economy and Technology Research Institute, Hohhot 010010, China (e-mail: 248349577@qq.com). Pareto optimal set (POS) which meets all system constraints. According to the commonly-used fuzzy affiliation function, the best compromise solution (BCS) of MOOPF problem can be determined from obtained POS set [5]. Then, adjusting the control variables based on the BCS of MOOPF problem can realize the desired operating state of power grids.

The non-convexity and high-dimensional characteristics make traditional methods unsuitable for MOOPF problems. While intelligent algorithms provide the effective way to solve this complex optimization problem. Now, the strength Pareto evolutionary algorithm [6], the cuckoo search algorithm [7], the novel hybrid bat algorithm [8] and the artificial fish swarm algorithm [2] published recently are all appropriate for solving MOOPF problems.

A. Contributions

Two main contributions, the improved NSGA-III (INSGA-III) algorithm and an effective BP fuel-cost prediction network, are put forward and applied to MOOPF problems.

1) INSGA-III Algorithm

In this paper, the NSGA-III algorithm, which is often regarded as one evaluation benchmark for multi-objective algorithms, is adopted to handle MOOPF problems. Since the relatively-scattered distribution of Pareto front (PF) obtained by the standard NSGA-III algorithm, the modified INSGA-III algorithm is put forward. The initial population of suggested INSGA-III algorithm is preliminarily screened by NSGA-II algorithm and the novel adaptive dominant (NAD) strategy is integrated into INSGA-III algorithm as well.

To validate the applicability of INSGA-III algorithm, two dual-objective and one triple-objective MOOPF experiments are conducted on the IEEE 30-node system. The generational distance (GD) and hyper-volume (HV) indexes quantitatively demonstrate that compared with the original NSGA-III algorithm, INSGA-III method has obvious advantages in PF-uniformity and PF-diversity. In addition, the suggested INSGA-III algorithm also achieves the higher-quality BCS solutions, which is conducive to the optimized operating status of power systems.

2) BP Fuel-cost Prediction Network

Furthermore, a fire new fuel-cost predicting model based on BP network is proposed to search the possible elite power-flow (EPL) solutions. Explored in a small range close to the current BCS, EPL solutions realize zero constraints violation and dominate the final BCS solution of INSGA-III method. Three experiments with different goal combinations prove that the presented BP fuel-cost prediction network is not only suitable for dual-objective MOOPF simulation problems, but also for the more complex triple-objective ones.

B. Structure

The structure of this paper is set as follows. Three goals and two kinds of constraints for MOOPF problems are given in Section II. Section III introduces two major contributions of this paper including INSGA-III algorithm and BP fuel-cost prediction model. Then, detailed results of three MOOPF cases to verify the superiority of INSGA-III algorithm and fuel-cost prediction model are given in Section IV. In the final, Section V gives the conclusion of this paper.

II. MOOPF MODEL

The mathematical model of MOOPF studied in this paper is mainly composed of three objective functions and system constraints.

A. Goals

The fuel cost (F_{cost}), power loss (F_{loss}) and emission (F_{emis}) are optimized by INSGA-III algorithm. The formulas of mentioned goals are shown as (1) ~ (3) [7, 9, 10].

$$F_{\cos t}(\$/h) = \sum_{i=1}^{N_G} (a_i + b_i P_{Gi} + c_i P_{Gi}^2)$$
(1)

$$F_{loss}(MW) = \sum_{k=1}^{N_L} c_k [V_i^2 + V_j^2 - 2V_i V_j \cos(\delta_i - \delta_j)]$$
(2)

$$F_{emis}(ton / h) = \sum_{i=1}^{N_G} [\alpha_i P_{Gi}^2 + \beta_i P_{Gi} + \gamma_i + \eta_i \exp(\lambda_i P_{Gi})] \quad (3)$$

where N_G , N_L are the numbers of generators and transmission lines. V_i and δ_i are the voltage-magnitude and voltage-angle of *i*th node. The other special symbols are clarified in literatures [5, 11, 12].

B. Constraints

The MOOPF problems are restricted by equality constraints and inequality ones.

1) Equality Constraints

Two equality constraints, the power balance equations in essence, are shown as (4) and (5) [13-15].

$$P_{Gi} - P_{Di} - V_i \sum_{j \in N_i} V_j (G_{ij} \cos \delta_{ij} + B_{ij} \sin \delta_{ij}) = 0, i \in N \quad (4)$$

$$Q_{Gi} - Q_{Di} - V_i \sum_{j \in N_i} V_j (G_{ij} \sin \delta_{ij} - B_{ij} \cos \delta_{ij}) = 0$$

$$i \in N_{PQ} \ \delta_{ij} = \delta_i - \delta_j$$
(5)

2) Inequality Constraints on Control Variables

The inequality restrictions on the generator node voltage (V_G) , the generator active power output at PV node (P_G) , the tap ratios of transformer (T) and the reactive power injection (Q_C) are shown as $(6) \sim (9)$ [5, 16].

$$V_{Gi}^{\min} \le V_{Gi} \le V_{Gi}^{\max}, \ i \in N_G \tag{6}$$

$$P_{Gi}^{\min} \le P_{Gi} \le P_{Gi}^{\max}, i \in N_G(i \neq 1)$$

$$\tag{7}$$

$$T_i^{\min} \le T_i \le T_i^{\max}, \ i \in N_T$$
(8)

$$Q_{Ci}^{\min} \le Q_{Ci} \le Q_{Ci}^{\max}, \ i \in N_C$$
(9)

3) Inequality Constraints on State Variables

The inequality restrictions on the generator active power at slack node (P_{G1}), the load node voltage (V_L), the generator reactive power (Q_G) and the apparent power of transmission line (S) are shown as (10) ~ (13) [1, 17].

$$P_{G1}^{\min} \le P_{G1} \le P_{G1}^{\max} \tag{10}$$

$$V_{Ii}^{\min} \le V_{Ii} \le V_{Ii}^{\max}, \ i \in N_{PQ}$$

$$\tag{11}$$

$$Q_{Gi}^{\min} \le Q_{Gi} \le Q_{Gi}^{\max}, \ i \in N_G$$
(12)

$$S_i^{\max} - S_i \ge 0, \ i \in N_I \tag{13}$$

where N_T , N_C , N_{PQ} are the numbers of transformers, compensators and PQ nodes. The other special symbols are clarified in literatures [5, 18, 19].

C. Constraints Processing

As the termination condition of Newton-Raphson power flow calculation, two equality constraints do not need the additional treatment. Therefore, this paper focuses on the processing of two kinds of inequality constraints.

1) Treatment of Unqualified Control Variables

The unqualified control variables which violate $(6) \sim (9)$ are regulated according to (14).

$$Con_{i} = \begin{cases} Con_{i}^{\max} & \text{if } Con_{i} > Con_{i}^{\max} \\ Con_{i}^{\min} & \text{if } Con_{i} < Con_{i}^{\min} \end{cases}$$
(14)

where Con_i^{max} indicates the maximum value of the *i*th control variables set and the Con_i^{min} is the minimal one.

2) Treatment of Unqualified State Variables

The unqualified state variables which violate $(10) \sim (13)$ will be filtered out based on the constraints-violation and objective-function values. The adoption priorities, also called the *Rank* index, of candidate power-flow schemes are determined according to (15) and (16). The acquisition of *Rank* is inspired by the non-inferior sorting idea proposed by Deb [20-22]. In detail, the *i*th power-flow solution will be given a higher adoption priority when condition (15) or (16) is met.

$$Cvio(S(Con_i)) < Cvio(S(Con_j))$$
 (15)

$$\begin{cases} Cvio(S(Con_i)) = Cvio(S(Con_j)) \\ Ob_m(S(Con_i)) \le Ob_m(S(Con_j)), \forall m \in \{1, 2, ..., N_o\} \ (16) \\ Ob_n(S(Con_i)) < Ob_n(S(Con_j)), \exists n \in \{1, 2, ..., N_o\} \end{cases}$$

where $Cvio(S(Con_i))$ defined as (17) is the constraints violation of the *i*th power-flow scheme. $Ob_m(S(Con_i))$ is the *m*th objective value of the *i*th power-flow scheme. Besides, N_o is the number of goals optimized simultaneously.

$$Cvio(S(Con_i)) = |Cvio_P(S(Con_i))| + |Cvio_V(S(Con_i))|$$
(17)

$$+ |Cvio_{\mathcal{Q}}(S(Con_i))| + |Cvio_{\mathcal{S}}(S(Con_i))|$$

where $Cvio_P(S(Con_i))$, $Cvio_V(S(Con_i))$, $Cvio_Q(S(Con_i))$ and $Cvio_S(S(Con_i))$ are the constraints violations of *i*th scheme which respectively violate (10) ~ (13).

III. ALGORITHM AND PREDICTION MODEL

The novel INSGA-III algorithm and BP fuel-cost prediction network, which are put forward to explore the satisfactory power flow scheduling schemes, are introduced as follows.

A. Modified INSGA-III Algorithm

The application of basic NSGA-III algorithm on MOOPF problems can refer to [5, 8, 23]. Aiming at the deficiencies of NSGA-III, two major measures are integrated into INSGA-III algorithm which greatly improve the performance for solving MOOPF problems.

1) Optimization of Initial Population

Due to the poor PF-distribution obtained by original NSGA-III method, an innovative idea of conducting the preliminary screening for initial population is put forward. In this paper, the typical NSGA-II algorithm is adopted to optimize the initial population of presented INSGA-III algorithm. The POS_{ns2} set obtained by NSGA-II method after $Ite_{ns2}(max)$ iterations is taken as the input of INSGA-III algorithm, which is helpful to make basic adjustments of PF-distribution at the initial stage.

2) NAD Dominant Strategy

In order to avoid the loss of high-quality power flow schemes, the proposed NAD dominant strategy is adopted in the iterative process of INSGA-III algorithm. The NAD strategy can be described as (18).

$$S_{k+1}^{valid}(Con_{i}) = \begin{cases} S_{k}^{valid}(Con_{i}), \\ if S_{k}^{valid}(Con_{i}) \ do \min ates \ S_{k+1}^{INSGA3}(Con_{i}) \\ S_{k+1}^{INSGA3}(Con_{i}), \\ if \ S_{k+1}^{INSGA3}(Con_{i}) \ do \min ates \ S_{k}^{valid}(Con_{i}) \end{cases}$$
(18)

where $S_{k+1}^{INSGA3}(Con_i)$ is the *i*th power flow solution updated based on INSGA-III model at the (k+1)th iteration. $S_{k+i}^{valid}(Con_i)$ indicates the final *i*th power flow solution of INSGA-III algorithm after the (k+1)th iteration.

In other word, the $S_k^{valid}(Con_i)$ will remain unchanged at the (k+1)th iteration when $S_{k+1}^{INSGA3}(Con_i)$ is not superior to $S_k^{valid}(Con_i)$. The dominant relationship of different schemes can be judged according to (15) and (16). The effective NAD strategy can reserve the elite power flow solutions to the great extent.

The main flow-chart of presented INSGA-III algorithm on MOOPF problems is summarized as Fig. 1. The $Ite_{ns3}(max)$ and POS_{ns3} indicate the maximum iteration and the final POS set of INSGA-III method. Additionally, the models of standard NSGA-III and NSGA-III algorithms can refer to [5, 20, 21].

B. BP Fuel-cost Prediction Model

In this paper, a novel BP fuel-cost prediction model, which is applicable for double-objective and triple-objective MOOPF problems, is proposed. Taking the basic fuel cost as the entry point, the proposed BP prediction model is able to search the EPL solutions near the current BCS solution of INSGA-III. The applications of neural network can refer to [24, 25].

The main steps of suggested fuel-cost prediction network are shown in TABLE I. In TABLE I, three indicators including the mean absolute error (MAE), the mean absolute percentage error (MAPE) and the root mean squared error (RMSE) are adopted to evaluate the performance of different predictive models. Three mentioned indexes are defined as (19) ~ (21) [26].



Fig. 1. Flow-chart of INSGA-III algorithm

$$MAE = \frac{1}{Ns} \sum_{i=1}^{Ns} \left| Fuel_{real}(i) - Fuel_{pre}(i) \right|$$
(19)

$$MAPE = \frac{1}{Ns} \sum_{i=1}^{Ns} \left| \frac{Fuel_{real}(i) - Fuel_{pre}(i)}{Fuel_{real}(i)} \right| \times 100\%$$
(20)

$$RMSE = \sqrt{\frac{\sum_{i=1}^{Ns} (Fuel_{real}(i) - Fuel_{pre}(i))^2}{Ns}}$$
(21)

where Ns is the population size of INSGA-III algorithm and $Fuel_{real}$ is the real fuel cost calculated by Newton-Raphson power flow method.

IV. EXPERIMENTS AND RESULTS

Three MOOPF cases on IEEE 30-node system with different goal combinations shown in TABLE II are studied. The structure of standard 30-node system is shown in Fig. 2 and the effective operating ranges of electrical equipment are clarified in [5, 27, 28].

	TABLE I	
MAIN STEPS OF	BP FUEL-COST P	REDICTION NETWORK

Ь	egin
	Input 2000 power flow scheduling schemes and the corresponding F_{cost} values;
	<i>for i</i> =1:5
	Select the random 1900 schemes for network-training (Input _{train}) and the other 100 schemes for testing (Input _{test});
	Identify the 1900 training-output (Output _{train}) and 100 testing-output (Output _{test});
	Perform the data normalization;
	% Clarify the structure of BP network
	$N_{BP(i)}$ =newff ($Input_{train}$, $Output_{train}$,[24,24]);
	$N_{BP(i)}$.trainParam.epochs=30;
	N _{BP(i)} .trainParam.lr=0.1;
	N _{BP(i)} .trainParam.goal=0.000001;
	Generate the <i>i</i> th candidate fuel-cost prediction network $N_{BP(i)}$;
	Predict the fuel cost of $Input_{test}$ set ($OutBP_{test}$) according to $N_{BP(i)}$ model;
	Perform the inverse-normalization on $OutBP_{test}$ set to obtain the predictive fuel cost value ($Fuel_{pre}$);
	Save the <i>i</i> th BP model $N_{BP(i)}$;
	end for
	Evaluate the quality of five BP fuel-cost models based on <i>Output_{test}</i> and <i>Fuel_{pre}</i> values;
	Determine the relatively-best model N_{BP}^{best} ;
	Sch _{all} =50;
	Sch_{elite} =10;
	Input the control variables set of BCS solution obtained by INSGA-III algorithm (C_{BCS}^{NSGA});
	Set the valid ranges of BP exploration within $[0.999C_{BCS}^{NSGA}, 1.001C_{BCS}^{NSGA}];$
	Randomly generate Schall control-variables sets within the valid ranges;
	Regulate the unqualified Sch _{all} sets based on (14);
	Obtain the $Fuel_{pre}$ values of Sch_{all} sets based on N_{BP}^{hest} network;
	Pick out the Schelite elite schemes with smaller Fuelpre values from Schall candidate schemes;
	Defense the Newton Decker a constitution to $C_{i}h_{i}$, where $c_{i}h_{i}$ is the real E_{i} E_{i} and E_{i} realized

Perform the Newton-Raphson power flow calculation to Sch_{elite} schemes and obtain the real F_{cost} , F_{emis} and F_{loss} values;

Determine the EPL solutions which dominate the current BCS from Schelite schemes;







A. Parameters

The influence of $Ite_{ns2}(max)$ and $Ite_{ns3}(max)$, two involved maximum iterations of INSGA-III algorithm, in solving MOOPF problems is firstly discussed.

Fig. 3 gives the PFs of CASE-1 with different maximum

iterations. It clearly indicates that the $Ite_{ns3}(max)=150$ ($Ite_{ns2}(max)=50$) only finds the feasible PF while $Ite_{ns3}(max)$ =150 ($Ite_{ns2}(max)=70$) achieves the relatively-optimal PF. In addition, Fig. 4 which gives the PFs of CASE-2 with different iterations also demonstrates INSGA-III algorithm can find the superior PF with $Ite_{ns3}(max)=150$ ($Ite_{ns2}(max)=70$). Therefore, it is reasonable to set the $Ite_{ns2}(max)$, $Ite_{ns3}(max)$ to 70 and 150, respectively.

The parameters of NSGA-II, which is used for the preliminary optimization of INSGA-III algorithm, can refer to [5]. Furthermore, the other parameters of proposed INSGA-III algorithm and the basic NSGA-III algorithm for comparison are set as TABLE III.

B. Verification Experiments

Massive results of three MOOPF cases are used to verify the applicability of INSGA-III method and BP prediction model.

1) CASE-1

The PFs of bi-objective CASE-1 obtained by traditional NSGA-III and modified INSGA-III algorithms are, respectively, given in Fig. 5 and Fig. 6. Intuitively, the PF-distribution of INSGA-III algorithm is much better than

the one of NSGA-III method.

Besides, the BCS and comparison results of CASE-1 are given in TABLE IV. TABLE IV shows that comparing with NSGA-III method, INSGA-III algorithm achieves the obviously smaller F_{cost} value with small differences in F_{emis} goal. Furthermore, the BCS solution of INSGA-III method including 0.2369 ton/h of F_{emis} and 831.6315 \$/h of F_{cost} dominates the ones of published MODFA and NHBA methods.

	TABLE II Case-setting		
Goal	CASE-1	CASE-2	CASE-3
F _{cost}	\checkmark		
F_{emis}	\checkmark		\checkmark
F_{loss}		\checkmark	\checkmark
Repeated number	30	30	30

TABI Algorithm I	le III Parameters	
Algorithm	NSGA-III	INSGA-III
Ns	100	100
$Ite_{ns2}(max)$	-	70
$Ite_{ns3}(max)$	300	150
mutation indictor/ percentage	20/1	20/1
crossover indictor/ percentage	20/0.1	20/0.1
number of divisions	10	10





Fig. 4. PF of CASE-2 with different iterations

Meanwhile, TABLE V gives the minimal F_{cost} and minimal F_{emis} of CASE-1. It indicates that the proposed INSGA-III algorithm finds 800.8147 \$/h of minimal F_{cost} and 0.1944 ton/h of minimal F_{emis} . In general, two minimal goals found by INSGA-III algorithm in CASE-1 are both superior to basic NSGA-III algorithm.

To quantitatively evaluate the PF-distribution and PF-diversity, the GD and HV indicators are adopted in this paper. The application of GD and HV indexes on MOOPF problems can refer to [5, 29]. In detail, the boxplots, the average and deviation of two related indictors for CASE-1 are given in Fig. 7 and TABLE VI. The smaller GD-average value shows the uniform-distribution of PF obtained by INSGA-III and the larger HV-average shows the better diversity. Then, the closer boxplot, the smaller GD and HV deviations prove the operational stability of INSGA-III algorithm.

More notably, five candidate BP predictive models which take the basic fuel cost as the entry-point are built for CASE-1. TABLE VII, which gives the MAE, MAPE, RMSE errors of five candidate models, indicates that the $N_{BP(5)}$ with three smaller errors achieves the relatively-best performance. Fig. 8 and Fig. 9, respectively, show the fitting results and relative error of CASE-1 based on $N_{BP(5)}$ network. It turns out the proposed BP fuel-cost model can effectively predict F_{cost} value based on the 24-dimensional control variables.



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	BCS	AND COMPARISON OF CASE-	1	
Variables	NSGA-III	CA INSGA-III	SE-1 MODFA [5]	NHBA [8]
P _{G2} (MW)	59.0446	60.3662	56.6689	58.1990
$P_{G5}(MW)$	27.8098	25.5531	28.2520	25.6741
P _{G8} (MW)	34.9985	35.0000	35.0000	27.0218
P _{G11} (MW)	27.3828	26.1379	26.3123	26.3626
$P_{G13}(MW)$	28.1427	23.8845	25.7403	31.3704
$V_{G1}(p.u.)$	1.0588	1.0411	1.0989	1.1000
$V_{G2}(p.u.)$	1.0457	1.0270	1.0909	1.0890
V _{G5} (p.u.)	1.0240	0.9873	1.0676	1.0537
V _{G8} (p.u.)	1.0269	0.9893	1.0804	1.0639
V _{G11} (p.u.)	1.0683	1.0571	1.0966	1.0880
V _{G13} (p.u.)	1.0861	1.0508	1.0999	1.0517
T ₁₁ (p.u.)	0.9999	0.9928	1.0151	1.0711
T ₁₂ (p.u.)	0.9007	0.9732	0.9493	0.9304
T ₁₅ (p.u.)	0.9759	0.9618	0.9903	1.1000
T ₃₆ (p.u.)	0.9370	0.9387	0.9666	1.0097
Q _{C10} (p.u.)	0.0022	0.0300	0.0000	0.0299
Q _{C12} (p.u.)	0.0341	0.0303	0.0423	0.0473
Q _{C15} (p.u.)	0.0000	0.0198	0.0463	0.0157
Q _{C17} (p.u.)	0.0045	0.0124	0.0462	0.0450
Q _{C20} (p.u.)	0.0201	0.0176	0.0243	0.0291
Q _{C21} (p.u.)	0.0302	0.0500	0.0421	0.0333
Q _{C23} (p.u.)	0.0478	0.0396	0.0415	0.0500
Q _{C24} (p.u.)	0.0454	0.0263	0.0198	0.0235
Q _{C29} (p.u.)	0.0477	0.0160	0.0198	0.0088
F_{emis} (ton/h)	0.2278	0.2369	0.2432	0.2375
$F_{cost}(h)$	839.1713	831.6315	831.6652	832.6471

TABLE V MINIMAL SOLUTIONS OF CASE-1

		CA	ASE-1	
Variables	Minim	al F _{cost}	Minima	al F _{emis}
	NSGA-III	INSGA-III	NSGA-III	INSGA-III
P _{G2} (MW)	50.9118	49.7022	72.6508	72.1929
P _{G5} (MW)	22.3327	21.4528	47.7526	50.0000
P _{G8} (MW)	32.5199	20.2328	34.9127	34.8866
P _{G11} (MW)	15.8096	13.0020	29.9436	30.0000
P _{G13} (MW)	22.5486	12.0609	40.0000	39.9993
V _{G1} (p.u.)	1.0628	1.0830	1.0566	1.0249
V _{G2} (p.u.)	1.0517	1.0630	1.0447	1.0157
V _{G5} (p.u.)	1.0152	1.0294	0.9907	0.9842
V _{G8} (p.u.)	1.0241	1.0352	1.0365	0.9840
V _{G11} (p.u.)	1.0251	1.0340	1.0400	1.0397
V _{G13} (p.u.)	1.0781	1.0677	1.0605	1.0119
T ₁₁ (p.u.)	0.9954	1.0147	0.9770	1.0104
T ₁₂ (p.u.)	0.9255	0.9343	0.9180	0.9781
T ₁₅ (p.u.)	1.0035	1.0757	1.0517	0.9485
T ₃₆ (p.u.)	0.9304	1.0080	0.9295	0.9518
Q _{C10} (p.u.)	0.0000	0.0306	0.0059	0.0339
Q _{C12} (p.u.)	0.0442	0.0216	0.0421	0.0361
Q _{C15} (p.u.)	0.0051	0.0414	0.0149	0.0268
Q _{C17} (p.u.)	0.0052	0.0369	0.0159	0.0071
Q _{C20} (p.u.)	0.0150	0.0281	0.0131	0.0158
Q _{C21} (p.u.)	0.0286	0.0233	0.0384	0.0467
Q _{C23} (p.u.)	0.0396	0.0199	0.0364	0.0472
Q _{C24} (p.u.)	0.0446	0.0269	0.0402	0.0282
Q _{C29} (p.u.)	0.0482	0.0488	0.0402	0.0353
F_{emis} (ton/h)	0.2743	0.3268	0.1952	0.1944
F_{cost} (\$/h)	810.7470	800.8147	944.2417	953.3882



		• 1
GD ANI	DHV OF	CASE-1

		G	D	Ц	W
Quantitative indicators		Average	Deviation	Average	Deviation
	NSGA-III	0.1241	0.0280	10.2723	0.3843
CASE-1	INSGA-III	0.0682	0.0132	17.8356	0.2914

	TABLE VII						
E	ERRORS OF C	ANDIDATE N	ETWORKS FO	DR CASE-1			
Networ	'ks	MAE	MAP	Έ	RMSE		
N _{BP(1})	0.0455	5.4167I	E-05	0.0836		
$N_{BP(2)}$		0.0593	7.0785I	E-05	0.0916		
N _{BP(3)}		0.0610	7.26721	E-05	0.0971		
$N_{BP(4)}$)	0.0599	7.1354I	E-05	0.1086		
N _{BP(5}	6)	0.0441	5.25331	E-05	0.0781		
			VIII				
	Sch _{elite} CANI	DIDATE ELITI	E SOLUTION	S OF CASE	-1		
Candidate	Solution ₁	$Solution_2$	Solution ₃	Solution ₄	$Solution_5$		
Fuel _{pre}	832.4020	832.4279	832.4353	832.4366	832.4415		
F_{cost}	831.5722	831.5168	831.6050	831.6046	831.6054		
F_{emis}	0.2369	0.2370	0.2370	0.2369	0.2370		
Dominance	\checkmark	-	-	\checkmark	-		
Candidate	Solution ₆	Solution7	Solution ₈	Solution ₉	Solution ₁₀		
$Fuel_{pre}$	832.4435	832.4438	832.4497	832.4513	832.4516		
F_{cost}	831.6101	831.5956	831.5835	831.5910	831.5606		
F_{emis}	0.2369	0.2370	0.2370	0.2369	0.2369		
Dominance	\checkmark	-	-	\checkmark	\checkmark		

Then, TABLE VIII gives the *Sch_{elite}* candidate elite solutions of CASE-1. It includes the predictive and real fuel cost, the real emission and the dominant relationship compared with the BCS of INSGA-III. It turns out five EPL solutions are determined by $N_{BP(5)}$ network.

In the end, five EPL solutions of CASE-1 which dominates the current BCS are given in TABLE IX. By adjusting the electrical devices based on the control variables of obtained EPL solutions, the more desirable grid operation state can be realized.

2) CASE-2

The PFs of another bi-objective CASE-2 obtained by NSGA-III and novel INSGA-III algorithms are given in Fig. 10 and Fig. 11, respectively. Fig. 11 shows comparing with NSGA-III, the suggested INSGA-III algorithm achieves the PF with better distribution-uniformity.

For CASE-2, the BCS solutions determined by NSGA-III, INSGA-III methods and the ones found by published NHBA,

HFBA-COFS algorithms are given in TABLE X. It indicates the BCS of INSGA-III method including 832.0140 \$/h of F_{cost} and 5.0766 MW of F_{loss} is more advantageous than the ones of NSGA-III and HFBA-COFS methods. For INSGA-III and NHBA algorithms, although the F_{loss} values obtained are similar, the former finds the significantly-smaller F_{cost} value.





V			CASE-1		
variables	EPL_1	EPL_2	EPL_3	EPL_4	EPL_5
P _{G2} (MW)	60.3738	60.3412	60.3425	60.3597	60.3235
P _{G5} (MW)	25.5367	25.5499	25.5757	25.5520	25.5764
P _{G8} (MW)	35.0000	35.0000	35.0000	34.9689	34.9788
P _{G11} (MW)	26.1245	26.1611	26.1309	26.1326	26.1237
P _{G13} (MW)	23.8720	23.8804	23.8662	23.9077	23.9031
V _{G1} (p.u.)	1.0407	1.0403	1.0406	1.04069	1.0415
V _{G2} (p.u.)	1.0277	1.0273	1.0276	1.0269	1.0269
V _{G5} (p.u.)	0.9879	0.9880	0.9878	0.9882	0.9882
V _{G8} (p.u.)	0.9898	0.9897	0.9893	0.9896	0.9900
V _{G11} (p.u.)	1.0579	1.0577	1.0569	1.0577	1.0577
V _{G13} (p.u.)	1.0517	1.0517	1.0513	1.0510	1.0501
T ₁₁ (p.u.)	0.9929	0.9927	0.9927	0.9928	0.9929
T ₁₂ (p.u.)	0.9732	0.9732	0.9732	0.9732	0.9733
T ₁₅ (p.u.)	0.9618	0.9618	0.9618	0.9618	0.9618
T ₃₆ (p.u.)	0.9387	0.9387	0.9387	0.9387	0.9387
Q _{C10} (p.u.)	0.0300	0.0300	0.0300	0.0300	0.0300
Q _{C12} (p.u.)	0.0303	0.0303	0.0303	0.0303	0.0303
Q _{C15} (p.u.)	0.0198	0.0198	0.0198	0.0198	0.0198
Q _{C17} (p.u.)	0.0124	0.0124	0.0124	0.0124	0.0124
Q _{C20} (p.u.)	0.0176	0.0176	0.0176	0.0176	0.0176
Q _{C21} (p.u.)	0.0500	0.0500	0.0500	0.0500	0.0500
Q _{C23} (p.u.)	0.0396	0.0396	0.0396	0.0396	0.0396
Q _{C24} (p.u.)	0.0263	0.0263	0.0263	0.0263	0.0263
Q _{C29} (p.u.)	0.0160	0.0160	0.0160	0.0160	0.0160
F_{cost} (\$/h)	831.5722	831.6046	831.6101	831.5910	831.5606
_{emis} (ton/h)	0.2369	0.2369	0.2369	0.2369	0.2369

CASE-2		ASE-2		
Variables	NSGA-III	INSGA-III	NHBA [8]	HFBA-COFS [29]
P _{G2} (MW)	53.7299	52.2117	54.7737	53.1358
P _{G5} (MW)	32.9401	30.0472	34.1273	32.4210
P _{G8} (MW)	34.9692	35.0000	35.0000	35.0000
P _{G11} (MW)	27.7402	29.8958	26.3571	26.5747
P _{G13} (MW)	23.7350	22.2722	20.5383	22.2063
V _{G1} (p.u.)	1.0851	1.1000	1.0993	1.1000
V _{G2} (p.u.)	1.0684	1.0874	1.0857	1.0881
V _{G5} (p.u.)	1.0432	1.0645	1.0629	1.0718
V _{G8} (p.u.)	1.0546	1.0729	1.0749	1.0767
V _{G11} (p.u.)	1.0941	1.1000	1.0754	1.0938
V _{G13} (p.u.)	1.0926	1.1000	1.0984	1.0951
T ₁₁ (p.u.)	0.9441	1.0285	0.9911	1.0304
T ₁₂ (p.u.)	1.0115	0.9098	0.9871	0.9469
T ₁₅ (p.u.)	0.9852	0.9803	0.9802	1.0078
T ₃₆ (p.u.)	0.9409	0.9709	0.9628	0.9818
Q _{C10} (p.u.)	0.0384	0.0082	0.0169	0.0489
Q _{C12} (p.u.)	0.0146	0.0500	0.0000	0.0314
Q _{C15} (p.u.)	0.0475	0.0203	0.0297	0.0324
Q _{C17} (p.u.)	0.0121	0.0362	0.0391	0.0460
Q _{C20} (p.u.)	0.0147	0.0462	0.0108	0.0265
Q _{C21} (p.u.)	0.0434	0.0494	0.0500	0.0249
Q _{C23} (p.u.)	0.0338	0.0449	0.0264	0.0421
Q _{C24} (p.u.)	0.0292	0.0434	0.0500	0.0424
Q _{C29} (p.u.)	0.0069	0.0491	0.0500	0.0457
F_{cost} (\$/h)	837.5766	832.0140	835.1034	832.3203
F_{loss} (MW)	5.0926	5.0766	5.0658	5.0796



 TABLE XI

 MINIMAL SOLUTIONS OF CASE-2

			CASE-2		
Variables	Minim	nal F _{cost}		Minimal Flos	55
	NSGA-III	INSGA-III		NSGA-III	INSGA-III
P _{G2} (MW)	51.1181	49.9739		60.2227	78.6055
P _{G5} (MW)	20.7737	22.2181		49.5555	50.0000
P _{G8} (MW)	32.8864	21.4304		34.2479	34.9974
P _{G11} (MW)	15.6043	11.6367		29.5579	29.9772
P _{G13} (MW)	15.2981	12.0003		39.2370	40.0000
V _{G1} (p.u.)	1.0967	1.0830		1.0703	1.0784
V _{G2} (p.u.)	1.0768	1.0668		1.0628	1.0706
V _{G5} (p.u.)	1.0504	1.0274		1.0440	1.0604
V _{G8} (p.u.)	1.0595	1.0401		1.0554	1.0642
V _{G11} (p.u.)	1.0816	1.0743		1.0997	1.0681
V _{G13} (p.u.)	1.0990	1.0991		1.0892	1.0581
T ₁₁ (p.u.)	0.9471	0.9725		0.9832	1.0520
T ₁₂ (p.u.)	1.0038	0.9698		0.9688	0.9588
T ₁₅ (p.u.)	0.9803	0.9581		0.9768	0.9824
T ₃₆ (p.u.)	0.9499	0.9894		0.9745	0.9949
Q _{C10} (p.u.)	0.0480	0.0250		0.0451	0.0346
Q _{C12} (p.u.)	0.0094	0.0078		0.0180	0.0280
Q _{C15} (p.u.)	0.0423	0.0403		0.0437	0.0415
Q _{C17} (p.u.)	0.0064	0.0085		0.0142	0.0099
Q _{C20} (p.u.)	0.0038	0.0479		0.0261	0.0240
Q _{C21} (p.u.)	0.0452	0.0455		0.0472	0.0274
Q _{C23} (p.u.)	0.0143	0.0212		0.0222	0.0369
Q _{C24} (p.u.)	0.0260	0.0394		0.0241	0.0242
Q _{C29} (p.u.)	0.0094	0.0449		0.0166	0.0263
Floss(MW)	7.4131	8.9075		3.3536	3.1271
F_{cost} (\$/h)	803.9893	800.6080		928.0639	964.6998
		TABLE XII GD and HV of CA	ASE-2		
0	• ••	GD)		HV
Quantitativ	e indicators	Average	Deviation	Average	Deviation
CASE 2	NSGA-III	0.0955	0.0216	617.3241	47.8720
CASE-2	INSGA-III	0.0808	0.0177	886 6208	42 7006

Additionally, the schemes with minimum single-objective of CASE-2 are shown in TABLE XI. The INSGA-III algorithm put forward in this paper obtains 800.6080 \$/h of minimal F_{cost} and 3.1271 MW of minimal F_{loss} . Both minimal F_{cost} and F_{loss} goals found by INSGA-III method are smaller than the ones found by NSGA-III, which verifies the competitive edge of INSGA-III in solving MOOPF problems.

Furthermore, Fig. 12 and TABLE XII show the evaluation results of PF-distribution and PF-diversity according to GD and HV criteria. In addition to verifying the advantages of INSGA-III algorithm in PF-uniformity and PF-diversity, the smaller GD-deviation and HV-deviation values also prove the better consistency of results from 30 MOOPF independent experiments.

Meanwhile, three related errors of five candidate BP fuel-cost models for CASE-2 are given in TABLE XIII. The $N_{BP(2)}$ network with relatively-minimal MAE, MAPE and RMSE errors is adopted to explore the preferable EPL solutions of CASE-2. Then, the fitting results and relative error corresponding to $N_{BP(2)}$ network are given in Fig. 13 and Fig. 14.

The detail of Sch_{elite} candidate elite solutions for CASE-2 are shown in TABLE XIV. It indicates that four EPL solutions are obtained by proposed $N_{BP(2)}$ fuel-cost forecasting network. And the control variables of EPL schemes are given in TABLE XV.

3) CASE-3

In CASE-3, F_{cost} , F_{loss} and F_{emis} goals are optimized at the same time. Obviously, the triple-goal MOOPF case is more difficult than the double-goal ones and it can further verify the performance of INSGA-III algorithm.

The PFs of CASE-3, which are respectively obtained by NSGA-III and INSGA-III algorithms, are shown in Fig. 15 and Fig. 16. Fig. 16 clearly states that the presented INSGA-III method is also able to find the satisfactory PF even in the triple-goal MOOPF case.

TABLE XIII Errors of Candidate Networks for CASE-2						
Networks		MAE	MAPE		RMSE	
$N_{BP(1)}$		0.0441	5.2512E	-05	0.0930	
$N_{BP(2)}$		0.0241	2.8809E-05		0.0362	
$N_{BP(3)}$		0.0373	4.4448E-05		0.0737	
$N_{BP(4)}$		0.0377	4.5000E-05		0.0538	
$N_{BP(5)}$		0.0576	6.8646E-05		0.1046	
TABLE XIV Schelie CANDIDATE ELITE SOLUTIONS OF CASE-2						
Candidate	te Solution ₁ Solution ₂ Solution ₃ Solution ₄ Solution					
Fuel _{pre}	831.5948	831.5999	831.6043	831.6077	831.6088	
F_{cost}	831.9510	831.9339	831.9426	831.9225	831.9401	
Floss	5.0827	5.0759	5.0755	5.0765	5.0832	
Dominance	-	\checkmark	\checkmark	\checkmark	-	
Candidate	Solution ₆	Solution7	Solution ₈	Solution ₉	Solution ₁₀	
Fuel _{pre}	831.6094	831.6129	831.6142	831.6262	831.6359	
F _{cost}	831.9504	831.9374	831.9460	831.9659	831.9667	
F _{loss}	5.0789	5.0804	5.0783	5.0819	5.0743	
Dominance	-	-	-	-		







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CASE-2						
Variables	EPL_1	EPL_2	EPL_3	EPL_4		
P _{G2} (MW)	52.2027	52.1697	52.1631	52.1698		
P _{G5} (MW)	30.0363	30.0300	30.0395	30.0503		
P _{G8} (MW)	35.0000	35.0000	35.0000	35.0000		
P _{G11} (MW)	29.8691	29.8798	29.8797	29.8801		
P _{G13} (MW)	22.2646	22.2869	22.2574	22.2779		
V _{G1} (p.u.)	1.1000	1.1000	1.1000	1.1000		
V _{G2} (p.u.)	1.0882	1.0881	1.0883	1.0884		
V _{G5} (p.u.)	1.0645	1.0647	1.0638	1.0638		
V _{G8} (p.u.)	1.0736	1.0734	1.0737	1.0733		
V _{G11} (p.u.)	1.0993	1.1000	1.1000	1.1000		
V _{G13} (p.u.)	1.1000	1.1000	1.0989	1.1000		
T ₁₁ (p.u.)	1.0286	1.0284	1.0285	1.0285		
T ₁₂ (p.u.)	0.9098	0.9098	0.9098	0.9098		
T ₁₅ (p.u.)	0.9803	0.9803	0.9803	0.9802		
T ₃₆ (p.u.)	0.9709	0.9709	0.9709	0.9710		
Q _{C10} (p.u.)	0.0082	0.0082	0.0082	0.0082		
Q _{C12} (p.u.)	0.0500	0.0500	0.0500	0.0500		
Q _{C15} (p.u.)	0.0203	0.0203	0.0203	0.0203		
Q _{C17} (p.u.)	0.0362	0.0362	0.0362	0.0362		
Q _{C20} (p.u.)	0.0462	0.0462	0.0462	0.0462		
Q _{C21} (p.u.)	0.0494	0.0494	0.0494	0.0494		
Q _{C23} (p.u.)	0.0449	0.0449	0.0449	0.0449		
Q _{C24} (p.u.)	0.0434	0.0434	0.0434	0.0434		
Q _{C29} (p.u.)	0.0491	0.0491	0.0491	0.0491		
F_{cost} (\$/h)	831.9339	831.9426	831.9225	831.9667		
F_{loss} (MW)	5.0759	5.0755	5.0765	5.0743		

CASE - 3 - NSGA-III

0.35 0.28 0.26 0.3 Emission (ton/h) Emission (ton/h) 0.24 0.25 0.22 0.2 0.2 0.15 0.18 10 8 8 1000 950 950 6 900 900 4 850 850 Power loss (MW) 2 Power loss (MW) 800 2 800 Fuel cost (\$/h) Fuel cost (\$/h) Fig. 15. PF of CASE-3 obtained by NSGA-III Fig. 16. PF of CASE-3 obtained by INSGA-III

TABLE XVI gives two BCS solutions and the comparison result found by the published MOFA-PFA method. The BCS of INSGA-III method composed by 876.9736 \$/h of F_{cost} , 4.2439 MW of F_{loss} and 0.2073 ton/h of F_{emis} is superior to the relatively-best scheme of typical NSGA-III. Besides, TABLE XVII shows the minimal F_{cost} (799.5961 \$/h), minimal F_{loss} (3.1242 MW), minimal F_{emis} (0.1943 ton/h) are all achieved by INSGA-III algorithm.

The errors of five fuel-cost prediction networks are shown in TABLE XVIII and the $N_{BP(3)}$ model with smaller MAE, MAPE, RMSE is finally adopted. For CASE-3, the fitting results and relative-error are, separately, given in Fig. 17 and Fig. 18.

CASE - 3 - INSGA-III

Furthermore, TABLE XIX gives the detail of Sch_{elite} candidate elite solutions of CASE-3. It intuitively states that five EPL solutions of CASE-3 are determined. Although the prediction effect of the tri-objective MOOPF case is not as good as that of the bi-objective one, the brand-new $N_{BP(3)}$ model still finds multiple EPL solutions. The control variables of five EPL scheme are shown in TABLE XX.

TABLE XVI BCS AND COMPARISON OF CASE-3					
variables	NSGA-III	INSGA-III	MOFA-PFA [30]		
P _{G2} (MW)	65.1562	61.4422	57.890		
P _{G5} (MW)	37.3055	37.1152	36.290		
P _{G8} (MW)	29.8221	34.0397	35.000		
P _{G11} (MW)	29.5921	29.7562	29.271		
P _{G13} (MW)	35.4797	35.8105	40.000		
V _{G1} (p.u.)	1.0343	1.0890	1.0985		
V _{G2} (p.u.)	1.02146	1.0788	1.0869		
V _{G5} (p.u.)	0.9952	1.0652	1.0625		
V _{G8} (p.u.)	1.0013	1.0673	1.0767		
V _{G11} (p.u.)	1.0231	1.0228	1.0857		
V _{G13} (p.u.)	1.0392	1.0387	1.0386		
T ₁₁ (p.u.)	1.0080	1.0535	1.0860		
T ₁₂ (p.u.)	0.9768	0.9129	0.9930		
T ₁₅ (p.u.)	1.0220	1.0199	1.0520		
T ₃₆ (p.u.)	0.9688	0.9846	1.0770		
Q _{C10} (p.u.)	0.0454	0.0428	0.0140		
Q _{C12} (p.u.)	0.0325	0.0203	0.020		
Q _{C15} (p.u.)	0.0050	0.0500	0.0080		
Q _{C17} (p.u.)	0.0278	0.0409	0.0250		
Q _{C20} (p.u.)	0.0223	0.0086	0.0390		
Q _{C21} (p.u.)	0.0087	0.0271	0.0270		
Q _{C23} (p.u.)	0.0294	0.0359	0.0100		
Q _{C24} (p.u.)	0.0500	0.0191	0.0170		
Q _{C29} (p.u.)	0.0130	0.0213	0.0500		
F_{cost} (\$/h)	878.1387	876.9736	879.91		
F_{loss} (MW)	4.7932	4.2439	4.2179		
F_{emis} (ton/h)	0.2092	0.2073	0.2165		

TABLE XVII MINIMAL SOLUTIONS OF CASE-3

			CASI	E-3			
Variables	Minimal <i>F</i> _{cost}		Minim	Minimal F _{loss}		Minimal F_{emis}	
	NSGA-III	INSGA-III	NSGA-III	INSGA-III	NSGA-III	INSGA-III	
P _{G2} (MW)	57.1339	48.4456	65.3614	79.3481	65.3614	72.7707	
P _{G5} (MW)	23.4779	21.5648	49.0766	50.0000	49.0766	50.0000	
P _{G8} (MW)	34.8481	22.2846	30.8966	35.0000	30.8966	35.0000	
P _{G11} (MW)	18.7528	11.8287	30.0000	29.5703	30.0000	30.0000	
P _{G13} (MW)	15.3990	12.0000	40.0000	40.0000	40.0000	40.0000	
V _{G1} (p.u.)	1.0541	1.1000	1.0236	1.0873	1.0236	1.0870	
V _{G2} (p.u.)	1.0389	1.0809	1.0154	1.0810	1.0154	1.0810	
V _{G5} (p.u.)	0.9862	1.0608	0.9883	1.0673	0.9883	1.0648	
V _{G8} (p.u.)	0.9986	1.0634	1.0090	1.0696	1.0090	1.0673	
V _{G11} (p.u.)	1.0410	1.0545	1.0366	1.0474	1.0366	1.0487	
V _{G13} (p.u.)	1.0173	1.0809	1.0485	1.0365	1.0485	1.0320	
T ₁₁ (p.u.)	0.9683	1.0896	0.9930	1.0734	0.9930	1.0715	
T ₁₂ (p.u.)	1.0375	0.9394	0.9926	0.9204	0.9926	0.9194	
T ₁₅ (p.u.)	0.9646	1.0151	0.9512	0.9989	0.9512	0.9859	
T ₃₆ (p.u.)	0.9551	1.0006	0.9214	1.0168	0.9214	1.0126	
Q _{C10} (p.u.)	0.0435	0.0496	0.0403	0.0412	0.0403	0.0420	
Q _{C12} (p.u.)	0.0305	0.0231	0.0301	0.0196	0.0301	0.0198	
Q _{C15} (p.u.)	0.0200	0.0324	0.0050	0.0463	0.0050	0.0462	
Q _{C17} (p.u.)	0.0419	0.0412	0.0325	0.0414	0.0325	0.0411	
Q _{C20} (p.u.)	0.0142	0.0080	0.0178	0.0110	0.0178	0.0111	
Q _{C21} (p.u.)	0.0240	0.0390	0.0174	0.0287	0.0174	0.0296	
Q _{C23} (p.u.)	0.0442	0.0375	0.0393	0.0361	0.0393	0.0361	
Q _{C24} (p.u.)	0.0406	0.0285	0.0500	0.0179	0.0500	0.0186	
Q _{C29} (p.u.)	0.0125	0.0124	0.0077	0.0206	0.0077	0.0220	
F_{cost} (\$/h)	813.1989	799.5961	932.9870	965.4179	932.9870	953.3341	
F_{loss} (MW)	7.5542	8.6646	3.9027	3.1242	3.9027	3.1834	
F_{emis} (ton/h)	0.2681	0.3268	0.1974	0.1950	0.1974	0.1943	



TABLE XVIII Errors of Candidate Networks for CASE-3							
Networks		MAE	MAPE		RMSE		
$N_{BP(1)}$	l)	0.1437	1.6644E-4		0.2688		
$N_{BP(2)}$	2)	0.1905	2.2066 E-4		0.2754		
N _{BP} (3	3)	0.0999	1.1562 E-4		0.1927		
N _{BP} (4	4)	0.1872	2.1683 E-4		0.4364		
N _{BP} (s	5)	0.1943	2.2498E-4		0.3287		
	TABLE XIX Scheihe CANDIDATE ELITE SOLUTIONS OF CASE-3						
Candidate	$Solution_1$	Solution ₂	Solution ₃	Solution ₄	$Solution_5$		
Fuel _{pre}	877.8448	877.8496	877.8514	877.8550	877.8553		
F_{cost}	876.9547	876.9620	876.9619	876.9630	876.9643		
F_{loss}	4.2442	4.2437	4.2452	4.2439	4.2445		
F_{emis}	0.2073	0.2073	0.2073	0.2073	0.2073		
Dominance	-	\checkmark	-	\checkmark	-		
Candidate	Solution ₆	Solution7	Solution ₈	Solution ₉	Solution ₁₀		
$Fuel_{pre}$	877.8589	877.8590	877.8591	877.8602	877.8602		
F_{cost}	876.9680	876.9685	876.9652	876.9714	876.9658		
F_{loss}	4.2435	4.2440	4.2438	4.2448	4.2427		

Fig. 18. Relative error of CASE-3

TABLE XX
EPL SOLUTIONS OF CASE-3

Femis

Dominance

0.2073

 $\sqrt{}$

0.2073

-

0.2073

 \checkmark

0.2073

-

0.2073

 $\sqrt{}$

\$7 . 11			CASE-3		
variables	EPL_1	EPL_2	EPL_3	EPL_4	EPL_5
P _{G2} (MW)	61.4413	61.4453	61.4445	61.4367	61.4419
P _{G5} (MW)	37.1136	37.1127	37.1155	37.1148	37.1118
P _{G8} (MW)	34.0383	34.0420	34.0366	34.0430	34.0411
P _{G11} (MW)	29.7559	29.7542	29.7550	29.7545	29.7587
P _{G13} (MW)	35.8090	35.8075	35.8093	35.8100	35.8103
V _{G1} (p.u.)	1.0890	1.0890	1.0891	1.0890	1.0890
V _{G2} (p.u.)	1.0789	1.0788	1.0788	1.0787	1.0789
V _{G5} (p.u.)	1.0652	1.0652	1.0651	1.0651	1.0651
V _{G8} (p.u.)	1.0672	1.0674	1.0673	1.0674	1.0674
V _{G11} (p.u.)	1.0228	1.0229	1.0228	1.0229	1.0228
V _{G13} (p.u.)	1.0387	1.0386	1.0388	1.0387	1.0388
T ₁₁ (p.u.)	1.0535	1.0535	1.0535	1.0535	1.0535
T ₁₂ (p.u.)	0.9129	0.9129	0.9129	0.9129	0.9129
T ₁₅ (p.u.)	1.0199	1.0199	1.0199	1.0199	1.0199
T ₃₆ (p.u.)	0.9846	0.9846	0.9846	0.9846	0.9846
Q _{C10} (p.u.)	0.0428	0.0428	0.0428	0.0428	0.0428
Q _{C12} (p.u.)	0.0203	0.0203	0.0203	0.0203	0.0203
Q _{C15} (p.u.)	0.0500	0.0500	0.0500	0.0500	0.0500
Q _{C17} (p.u.)	0.0409	0.0409	0.0409	0.0409	0.0409
Q _{C20} (p.u.)	0.0086	0.0086	0.0086	0.0086	0.0086
Q _{C21} (p.u.)	0.0271	0.0271	0.0271	0.0271	0.0271
Q _{C23} (p.u.)	0.0359	0.0359	0.0359	0.0359	0.0359
Q _{C24} (p.u.)	0.0191	0.0191	0.0191	0.0191	0.0191
Q _{C29} (p.u.)	0.0213	0.0213	0.0213	0.0213	0.0213
F_{cost} (\$/h)	876.9620	876.9630	876.9680	876.9652	876.9658
F_{loss} (MW)	4.2437	4.2439	4.2435	4.2438	4.2427
F_{emis} (ton/h)	0.2073	0.2073	0.2073	0.2073	0.2073

It is very difficult to find the EPL solutions with all three goals smaller than the current BCS. Thrillingly, the presented BP fuel-cost model can effectively solve the mentioned difficulties.

V. CONCLUSION

To explore the high-performance scheduling schemes with zero constraints-violation, the modified INSGA-III algorithm and an innovative fuel-cost forecasting network are proposed. Combining with NAD dominant strategy, the presented INSGA-III algorithm achieves the evenly-distributed PFs. Furthermore, the novel BP fuel-cost prediction model is put forward and it successfully finds more than four EPL solutions near the current BCS solution. Numerous results strongly prove the applicability and advantages of proposed INSGA-III algorithm and BP fuel-cost model in both double-goal and triple-goal MOOPF problems.

In conclusion, the advanced computer technologies such as neural networks and intelligence algorithms offer another powerful way to handle the complex MOOPF problems.

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