

Punctual State Computation Using Discrete Modeling

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Abstract—The paper proposes a sequential computation method of the state vector associated to a circuit in dynamic behavior, for pre-established time intervals or punctually. Based on discrete circuit models with direct or iterative companion diagrams, the method is intended to a wide range of analog circuits: linear or nonlinear circuits, with or without magnetically coupled inductors or excess elements. The enclosed example proves the efficiency and the accessibility of the proposed analysis method.

Index Terms—Analog circuit, discrete modeling, numerical integration, state variable formulation.

I. INTRODUCTION

The discretization of the circuit elements, followed by corresponding companion diagrams, leads to discrete circuit models associated to the analyzed analog circuits [1,2]. Using the Euler, trapezoidal or Gear approximations [3,4], simple discretized models are generated, whose implementation leads to an auxiliary active resistive network. In this manner, the numerical computation of desired dynamic quantities becomes easier and faster. Considering the time constants of the circuit, the discretization time step can be adjusted for reaching the solution optimally, in terms of precision and computation time.

The discrete modeling of nonlinear circuits assumes an iterative process too, that requires updating the parameters of the companion diagram at each iteration and each integration time step [4,5]. If nonzero initial conditions exist, they are computed usually through a steady state analysis performed prior to the transient analysis.

The discrete modeling can be associated to the state variables approach [6,7], as well as the modified nodal approach [4,8], the analysis strategy being chosen in accordance with the circuit topology, the number of the energy storage circuit elements (capacitors and inductors) and the global size of the circuit.

The known computation algorithms based on the discrete modeling allow the sequential computation, step by step, along the whole analysis time, of the state vector or output vector directly [4,9]. In this paper, one proposes a method that allows computing the state vector punctually, at the moments considered significant for the dynamic evolution of the circuit. Thus, the sequential computation for pre-established time subdomains is allowed.

II. MODELING THROUGH COMPANION DIAGRAMS

The time domain analysis is performed for the time interval $[t_0, t_f]$, bounded by the initial moment t_0 and the final moment t_f . It can be discretized with the constant time step h , chosen sufficiently small in order to allow using the Euler, trapezoidal or Gear numerical integration algorithms [1-4]. One can choose $t_0 = 0$ and $t_f = wh$, where w is a positive integer.

The analog circuit analysis using discrete models requires replacing each circuit element through a proper model according to its constitutive equations. In this way, if the Euler approximation is used, the discretization equations and the corresponding discrete circuit models associated to the energy storage circuit elements are shown in table 1, for the time interval $[nh, (n+1)h]$, $h < w$.

The tree capacitor voltages \mathbf{u}_C and the cotree inductor currents \mathbf{i}_L [6,7] are chosen as state quantities, assembled in the state vector \mathbf{x} . The currents \mathbf{I}_C of the tree capacitors and the voltages across the cotree inductors \mathbf{U}_L are complementary variables, assembled in the vector \mathbf{X} .

At the moment $t = nh$, the above named vectors are partitioned as:

$$\mathbf{x}^n = \begin{bmatrix} \mathbf{u}_C^n \\ \mathbf{i}_L^n \end{bmatrix}, \quad \mathbf{X}^n = \begin{bmatrix} \mathbf{I}_C^n \\ \mathbf{U}_L^n \end{bmatrix} \quad (1)$$

with obvious significances of the vectors $\mathbf{u}_C^n, \mathbf{i}_L^n, \mathbf{I}_C^n, \mathbf{U}_L^n$.

For the magnetically coupled inductors, the discretized equations and the companion diagram are shown in table 1, where the following notations were used:

$$\begin{aligned} R_{11}^{n+1} &= \frac{L_{11}}{h}, R_{12}^{n+1} = \frac{L_{12}}{h}, e_1^{n+1} = \frac{L_{11}}{h} i_1^n + \frac{L_{12}}{h} i_2^n, \\ R_{22}^{n+1} &= \frac{L_{22}}{h}, R_{21}^{n+1} = \frac{L_{21}}{h}, e_2^{n+1} = \frac{L_{22}}{h} i_2^n + \frac{L_{21}}{h} i_1^n. \end{aligned} \quad (2)$$

For nonlinear circuits, the state variable computation at the moment $t = (n+1)h$ requires an iterative process that converges towards the exact solution [4,5]. A second upper index corresponds to the iteration order (see table 2). Similar results to those of table 1 and table 2 can be obtained using the trapezoidal [4,10] or Gear integration rule [3,4].

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Table I: Discrete modeling of the energy storage elements.

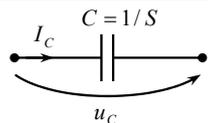
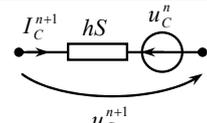
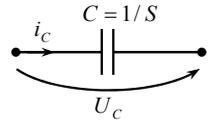
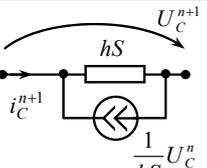
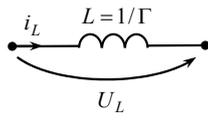
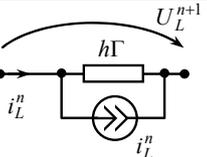
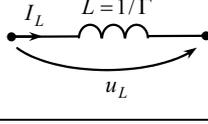
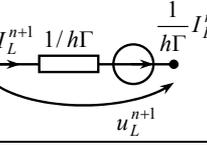
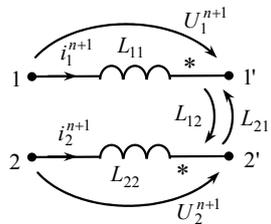
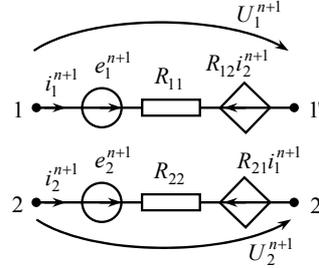
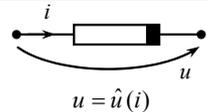
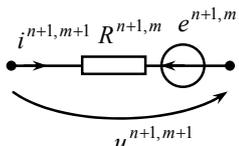
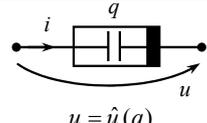
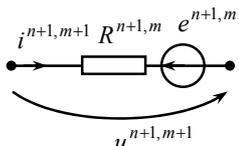
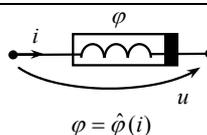
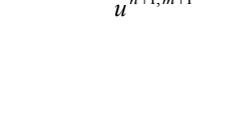
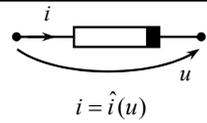
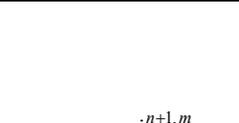
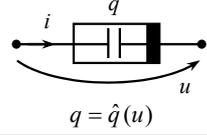
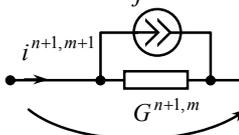
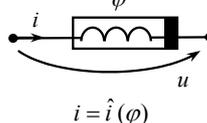
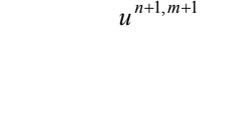
No.	Element	Symbol	Discretized expressions	Companion diagram
1	Tree capacitor		$u_C^{n+1} = u_C^n + hSI_C^{n+1}$	
2	Excess capacitor		$i_C^{n+1} = \frac{1}{hS}(U_C^{n+1} - U_C^n)$	
3	Cotree inductor		$i_L^{n+1} = i_L^n + h\Gamma U_L^{n+1}$	
4	Excess inductor		$u_L^{n+1} = \frac{1}{h\Gamma}(I_L^{n+1} - I_L^n)$	
5	Magnetically coupled inductor pair		$U_1^{n+1} = R_{11}i_1^{n+1} - R_{11}i_1^n + R_{12}i_2^{n+1} - R_{12}i_2^n$ $U_2^{n+1} = R_{21}i_1^{n+1} - R_{21}i_1^n + R_{22}i_2^{n+1} - R_{22}i_2^n$	

Table II: Iterative discrete modeling.

No.	Element	Iterative dynamic parameter	Companion diagram	Notations in the companion diagram
1		$R^{n+1,m} = \left(\frac{\partial u}{\partial i}\right)_{i=i^{n+1,m}}$		$R^{n+1,m} = R^{n+1,m}$ $e^{n+1,m} = u^{n+1,m} - R^{n+1,m} \cdot i^{n+1,m}$
2		$C^{n+1,m} = \left(\frac{\partial q}{\partial u}\right)_{u=u^{n+1,m}}$		$R^{n+1,m} = hS^{n+1,m}$ $e^{n+1,m} = u^{n+1,m} - hS^{n+1,m} \cdot i^{n+1,m}$
3		$L^{n+1,m} = \left(\frac{\partial \varphi}{\partial i}\right)_{i=i^{n+1,m}}$		$R^{n+1,m} = \frac{1}{h} L^{n+1,m}$ $e^{n+1,m} = u^{n+1,m} - \frac{1}{h} L^{n+1,m} \cdot i^{n+1,m}$
4		$G^{n+1,m} = \left(\frac{\partial i}{\partial u}\right)_{u=u^{n+1,m}}$		$G^{n+1,m} = G^{n+1,m}$ $j^{n+1,m} = i^{n+1,m} - G^{n+1,m} \cdot u^{n+1,m}$
5		$S^{n+1,m} = \left(\frac{\partial u}{\partial q}\right)_{q=q^{n+1,m}}$		$G^{n+1,m} = \frac{1}{h} C^{n+1,m}$ $j^{n+1,m} = i^{n+1,m} - \frac{1}{h} C^{n+1,m} \cdot u^{n+1,m}$
6		$\Gamma^{n+1,m} = \left(\frac{\partial i}{\partial \varphi}\right)_{\varphi=\varphi^{n+1,m}}$		$G^{n+1,m} = h\Gamma^{n+1,m}$ $j^{n+1,m} = i^{n+1,m} - h\Gamma^{n+1,m} \cdot u^{n+1,m}$

III. SEQUENTIAL AND PUNCTUAL STATE COMPUTATION

The treatment with discretized models assumes substituting the circuit elements with companion diagrams, which consist in a resistive model diagram. It allows the sequential computation of the circuit solution.

A. Circuits without excess elements

If the given circuit does not contain capacitor loops nor inductor cutsets [6,7], the discretization expressions associated to the energy storage elements (table 1, lines 1 and 3), using the notations (1), one obtains

$$\mathbf{x}^{n+1} = \mathbf{x}^n + h \begin{bmatrix} \mathbf{S} & \mathbf{0} \\ \mathbf{0} & \mathbf{\Gamma} \end{bmatrix} \mathbf{x}^{n+1}, \quad (3)$$

where \mathbf{S} is the diagonal matrix of capacitor elastances and $\mathbf{\Gamma}$ is the matrix of inductor reciprocal inductances.

Starting from the companion resistive diagram, the complementary variables are obtained as output quantities [4,9,10] of the circuit

$$\mathbf{X}^{n+1} = \mathbf{E} \mathbf{x}^n + \mathbf{F} \mathbf{u}^{n+1}, \quad (4)$$

where \mathbf{E} and \mathbf{F} are transmittance matrices, and \mathbf{u}^{n+1} is the vector of input quantities [4,6,7] at the moment $t = (n+1)h$.

From (3) and (4) one obtains an equation that allows computing the state vector sequentially, starting from its initial value $\mathbf{x}^0 = \mathbf{x}(0)$ until the final value $\mathbf{x}^w = \mathbf{x}(wh)$:

$$\mathbf{x}^{n+1} = \mathbf{M} \mathbf{x}^n + \mathbf{N} \mathbf{u}^{n+1}, \quad (5)$$

where

$$\mathbf{M} = \mathbf{1} + h \begin{bmatrix} \mathbf{S} & \mathbf{0} \\ \mathbf{0} & \mathbf{\Gamma} \end{bmatrix} \mathbf{E}, \quad (6)$$

$\mathbf{1}$ being the identity matrix, and

$$\mathbf{N} = h \begin{bmatrix} \mathbf{S} & \mathbf{0} \\ \mathbf{0} & \mathbf{\Gamma} \end{bmatrix} \mathbf{F}. \quad (7)$$

Starting from eq. (5), through mathematical induction, the useful formula is obtained as

$$\mathbf{x}^n = \mathbf{M}^n \mathbf{x}^0 + \sum_{i=1}^n \mathbf{M}^{n-i} \mathbf{N} \mathbf{u}^i, \quad (8)$$

where the upper indexes of the matrix \mathbf{M} are integer power exponents. The formula (8) allows the punctual computation of the state vector at any moment $t = nh$, if the initial conditions of the circuit and the excitation quantities are known.

If a particular solution $\mathbf{x}_p(t)$ of the state equation exists, it significantly simplifies the computation of the general

solution $\mathbf{x}(t)$. Using the Euler numerical integration method, one obtains [4]:

$$\mathbf{x}^{n+1} = \mathbf{M}(\mathbf{x}^n - \mathbf{x}_p^n) + \mathbf{x}_p^{n+1}. \quad (9)$$

The sequentially computation of the state vector implies the priory construction of the matrix \mathbf{E} , according to eq. (6) and (9). This action requires analyzing an auxiliary circuit obtained by setting all independent sources to zero in the given circuit.

Starting from eq. (9), the expression

$$\mathbf{x}^n = \mathbf{M}^n(\mathbf{x}^0 - \mathbf{x}_p^0) + \mathbf{x}_p^n \quad (10)$$

allows the punctual computation of the state vector.

B. Circuits with excess elements

The excess capacitor voltages [6,7,10], assembled in the vector \mathbf{U}_C , as well as the excess inductor currents [4,6,7], assembled in the vector \mathbf{I}_L , can be expressed in terms of the state variables and excitation quantities, at the moment $t = nh$:

$$\begin{bmatrix} \mathbf{U}_C^n \\ \mathbf{I}_L^n \end{bmatrix} = \begin{bmatrix} \mathbf{K}_1 & \mathbf{0} \\ \mathbf{0} & \mathbf{K}_2 \end{bmatrix} \mathbf{x}^n + \begin{bmatrix} \mathbf{K}_1' & \mathbf{0} \\ \mathbf{0} & \mathbf{K}_2' \end{bmatrix} \mathbf{u}^n, \quad (11)$$

where the matrices $\mathbf{K}_1, \mathbf{K}_1'$ and $\mathbf{K}_2, \mathbf{K}_2'$ contain voltage and current ratios respectively.

Using the table 1, the companion diagram associated to the analyzed circuit can be obtained, whence the complementary quantities are given by:

$$\mathbf{X}^{n+1} = \mathbf{E} \mathbf{x}^n + \mathbf{E}_1 \begin{bmatrix} \mathbf{U}_C^n \\ \mathbf{I}_L^n \end{bmatrix} + \mathbf{F} \mathbf{u}^n, \quad (12)$$

the matrices \mathbf{E}, \mathbf{E}_1 and \mathbf{F} containing transmittance coefficients.

Considering eq. (11) and (12), the recurrence expression is obtained from (5), allowing the sequential computation of the state vector:

$$\mathbf{x}^{n+1} = \mathbf{M} \mathbf{x}^n + \mathbf{N} \mathbf{u}^{n+1} + \mathbf{N}_1 \mathbf{u}^n, \quad (13)$$

where

$$\begin{aligned} \mathbf{M} &= \mathbf{1} + h \begin{bmatrix} \mathbf{S} & \mathbf{0} \\ \mathbf{0} & \mathbf{\Gamma} \end{bmatrix} (\mathbf{E} + \mathbf{E}_1 \mathbf{K}), \\ \mathbf{N} &= h \begin{bmatrix} \mathbf{S} & \mathbf{0} \\ \mathbf{0} & \mathbf{\Gamma} \end{bmatrix} \mathbf{F}, \quad \mathbf{N}_1 = h \begin{bmatrix} \mathbf{S} & \mathbf{0} \\ \mathbf{0} & \mathbf{\Gamma} \end{bmatrix} \mathbf{E}_1 \mathbf{K}', \\ \mathbf{K} &= \begin{bmatrix} \mathbf{K}_1 & \mathbf{0} \\ \mathbf{0} & \mathbf{K}_2 \end{bmatrix}, \quad \mathbf{K}' = \begin{bmatrix} \mathbf{K}_1' & \mathbf{0} \\ \mathbf{0} & \mathbf{K}_2' \end{bmatrix}. \end{aligned} \quad (14)$$

If \mathbf{x}_p is a particular solution of the state equation, the following identity is obtained:

$$N \mathbf{u}^{n+1} + N_1 \mathbf{u}^n = \mathbf{x}_p^{n+1} - M \mathbf{x}_p^n, \quad (15)$$

that allows converting (13) in the form (9), as common expression for any circuit (with or without excess elements).

IV. EXAMPLE

In order to exemplify the above described algorithm, let us consider the transient response of the circuit shown in fig. 1, caused by turning on the switch. The circuit parameters are:

$$\begin{aligned} R_1 = R_2 = R_3 &= 10\Omega; \\ L &= 10\text{mH}; C = 100\mu\text{F}; \\ E &= 10\text{V}; J = 1\text{A}. \end{aligned}$$

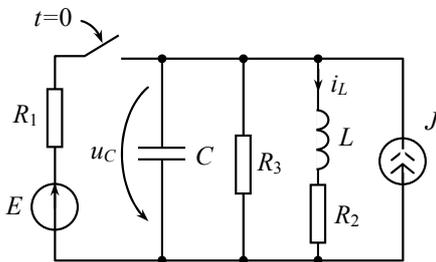


Fig. 1. Circuit example.

The time-response of capacitor voltage and inductor current will be computed for the time interval $t \in [0, 5\text{ms}]$. These quantities are the state variables too. The corresponding discretized Euler companion diagram is shown in fig. 2.

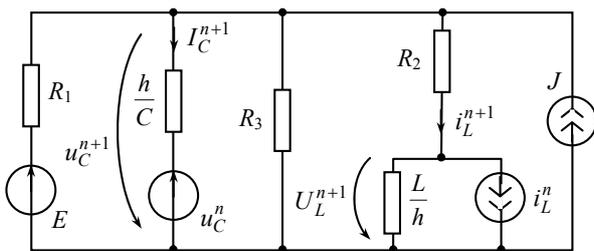


Fig. 2. Discretized diagram.

According to the notations used in section II, we have:

$$\mathbf{x} = \begin{bmatrix} u_C \\ i_L \end{bmatrix}; \quad \mathbf{X} = \begin{bmatrix} I_C \\ U_L \end{bmatrix}; \quad \mathbf{u} = \begin{bmatrix} E \\ J \end{bmatrix}$$

The computation way of the matrices \mathbf{E} and \mathbf{F} arises from the particular form of the expression (4):

$$\begin{bmatrix} I_C^{n+1} \\ U_L^{n+1} \end{bmatrix} = \begin{bmatrix} e_{11} & e_{12} \\ e_{21} & e_{22} \end{bmatrix} \cdot \begin{bmatrix} u_C^n \\ i_L^n \end{bmatrix} + \begin{bmatrix} f_{11} & f_{12} \\ f_{21} & f_{22} \end{bmatrix} \cdot \begin{bmatrix} E \\ J \end{bmatrix}$$

from where:

$$e_{11} = \left. \frac{I_C^{n+1}}{u_C^n} \right|_{i_L^n=0; E=0; J=0}; \quad e_{12} = \left. \frac{I_C^{n+1}}{i_L^n} \right|_{u_C^n=0; E=0; J=0};$$

$$e_{21} = \left. \frac{U_L^{n+1}}{u_C^n} \right|_{i_L^n=0; E=0; J=0}; \quad e_{22} = \left. \frac{U_L^{n+1}}{i_L^n} \right|_{u_C^n=0; E=0; J=0};$$

$$f_{11} = \left. \frac{I_C^{n+1}}{E} \right|_{u_C^n=0; i_L^n=0; J=0}; \quad f_{12} = \left. \frac{I_C^{n+1}}{J} \right|_{u_C^n=0; i_L^n=0; E=0};$$

$$f_{21} = \left. \frac{U_L^{n+1}}{E} \right|_{u_C^n=0; i_L^n=0; J=0}; \quad f_{22} = \left. \frac{U_L^{n+1}}{J} \right|_{u_C^n=0; i_L^n=0; E=0}.$$

Using the diagram of fig. 2, the elements of the matrices \mathbf{E} and \mathbf{F} were computed, assuming a constant time step $h = 0.1\text{ms}$:

$$\mathbf{E} = \begin{bmatrix} -0,1729 & -0,7519 \\ 0,7519 & -9,7740 \end{bmatrix}, \quad \mathbf{F} = \begin{bmatrix} 0,0827 & 0,8270 \\ 0,0752 & 0,7519 \end{bmatrix}$$

The matrices \mathbf{M} and \mathbf{N} given by eq. (6), (7) are:

$$\begin{aligned} \mathbf{M} &= \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} + 0,1 \cdot 10^{-3} \cdot \begin{bmatrix} \frac{1}{100 \cdot 10^{-6}} & 0 \\ 0 & \frac{1}{10 \cdot 10^{-3}} \end{bmatrix} \cdot \mathbf{E} = \\ &= \begin{bmatrix} 0,8271 & -0,7519 \\ 0,0075 & 0,9023 \end{bmatrix}, \end{aligned}$$

$$\mathbf{N} = 0,1 \cdot 10^{-3} \cdot \begin{bmatrix} \frac{1}{100 \cdot 10^{-6}} & 0 \\ 0 & \frac{1}{10 \cdot 10^{-3}} \end{bmatrix} \cdot \mathbf{F} = \begin{bmatrix} 0,0827 & 0,8270 \\ 0,0008 & 0,0075 \end{bmatrix}.$$

Starting from the obvious initial condition

$$\mathbf{x}^0 = \begin{bmatrix} u_C^0 \\ i_L^0 \end{bmatrix} = \begin{bmatrix} 5\text{V} \\ 0,5\text{A} \end{bmatrix},$$

the solutions were computed using (8) and represented in fig. 3 with solid line.

The calculus was repeated in the same manner for a longer time step, $h' = 5h = 0,5\text{ms}$, the solution being shown in the same figure. Both computed solutions are referred to the exact solution represented with thin dashed line.

V. CONCLUSION

The proposed analysis strategy and computation formulae allow not only the punctual computation of the state vector, but also allow crossing the integration subdomains with variable time step. The proposed method harmonizes naturally with any procedure based on discrete models of analog circuits, including the methods for iterative

computation of nonlinear dynamic networks.

The versatility of the method has already allowed an extension, in connection to the modified nodal approach.

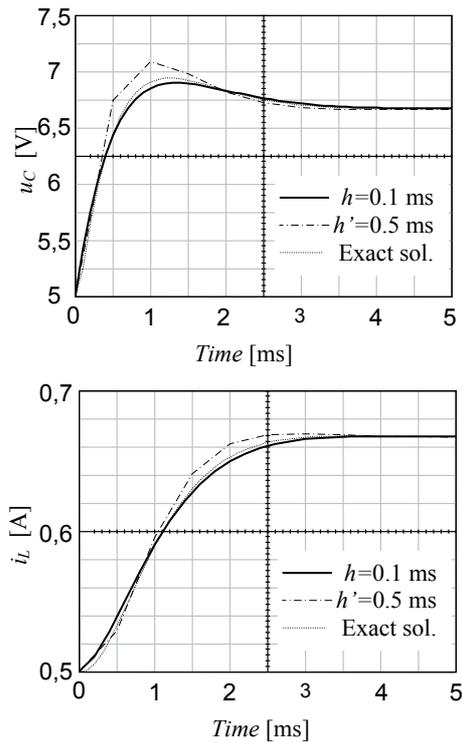


Fig. 3. Circuit response.

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